Scotia Drilling Continues to Support Growth

Pantoro Gold Limited (**ASX:PNR**) (**Pantoro Gold** or the **Company**), a WA-based gold producer focused on unlocking the full potential of its 100%-owned Norseman Gold Project (**Norseman** or the **Project**), is pleased to provide an update on the ongoing underground and surface diamond drilling program at the Scotia Underground Mine.

Key Highlights

- Extensional drilling in Central Scotia has confirmed wide, high-grade mineralisation extending at least 50 metres below the current Scotia Indicated Mineral Resource and remains open at depth supporting the potential for additional development levels beyond the existing mine plan.
- Grade control drilling has returned multiple high-grade intersections within the current mine plan across the Scotia North and Taurus orebodies.
- The Company has approved additional levels outside of the current mine plan further extending mine life.

Central Scotia

» 16.09 m @ 10.59 g/t Au including 1.58 m @ 30.48 g/t Au, and 1.75 m @ 41.72 g/t Au, and 1.31 m @ 18.02 g/t Au.
» 10.29 m @ 6.31 g/t Au including 3.28 m @ 15.78 g/t Au.
» 10.48 m @ 6.74 g/t Au including 1.01 m @ 9.99 g/t Au and, 0.94 m @ 23.21 g/t Au, and 1 m @ 29.17 g/t Au.
» 7.05 m @ 11.2 g/t Au including 0.93 m @ 25.46 g/t Au and 0.92 m @ 55.28 g/t Au.
» 3.52 m @ 49.82 g/t Au including 1.69 m @ 102.44 g/t Au.
» 2.24 m @ 21.13 g/t Au including 0.55 m @ 67.44 g/t Au.
» 3.11 m @ 8.26 g/t Au including 0.83 m @ 30.33 g/t Au.
» 0.45 m @ 66.15 g/t Au.
» 3.52 m @ 49.82 g/t Au including 1.69 m @ 102.44 g/t Au.

Scotia North

» 3.35 m @ 14.82 g/t Au including 2.7 m @ 18.11 g/t Au.
» 4.31 m @ 8.89 g/t Au including 1.45 m @ 18.78 g/t Au.
» 3.08 m @ 6.21 g/t Au including 0.86 m @ 10.98 g/t Au.
» 5.84 m @ 3.42 g/t Au including 0.79 m @ 8.41 g/t Au and 0.87 m @ 6.36 g/t Au.
» 3.07 m @ 11.92 g/t Au including 0.83 m @ 37.67 g/t Au.
» 1.75 m @ 11.91 g/t Au including 0.37 m @ 48.77 g/t Au and 0.38 m @ 6.41 g/t Au.

Scotia South

» 2.7 m @ 25.15 g/t Au including 0.36 m @ 59.29 g/t Au and 0.62 m @ 49.67 g/t Au.

Taurus

Taurus is a northern extension to the Scotia orebody and is included in the current mine plan.

» 4.8 m @ 15.57 g/t Au including 0.76 m @ 42.12 g/t Au and 1 m @ 28.88 g/t Au.

Commenting on the results, Pantoro Gold Managing Director Paul Cmrlec said:

"Development at Scotia North is now opening up new mineralisation for production, meaningfully improving production flexibility at the mine. These high-grade infill results, combined with the continued resource growth at Central Scotia and Scotia South, position the mine to grow its production in FY2027.

While development and production have run behind schedule due to a number of factors in FY2026, the orebody continues to impress. We remain confident that Scotia will deliver years of high-grade ore feed to Norseman as these additional areas come into full production."

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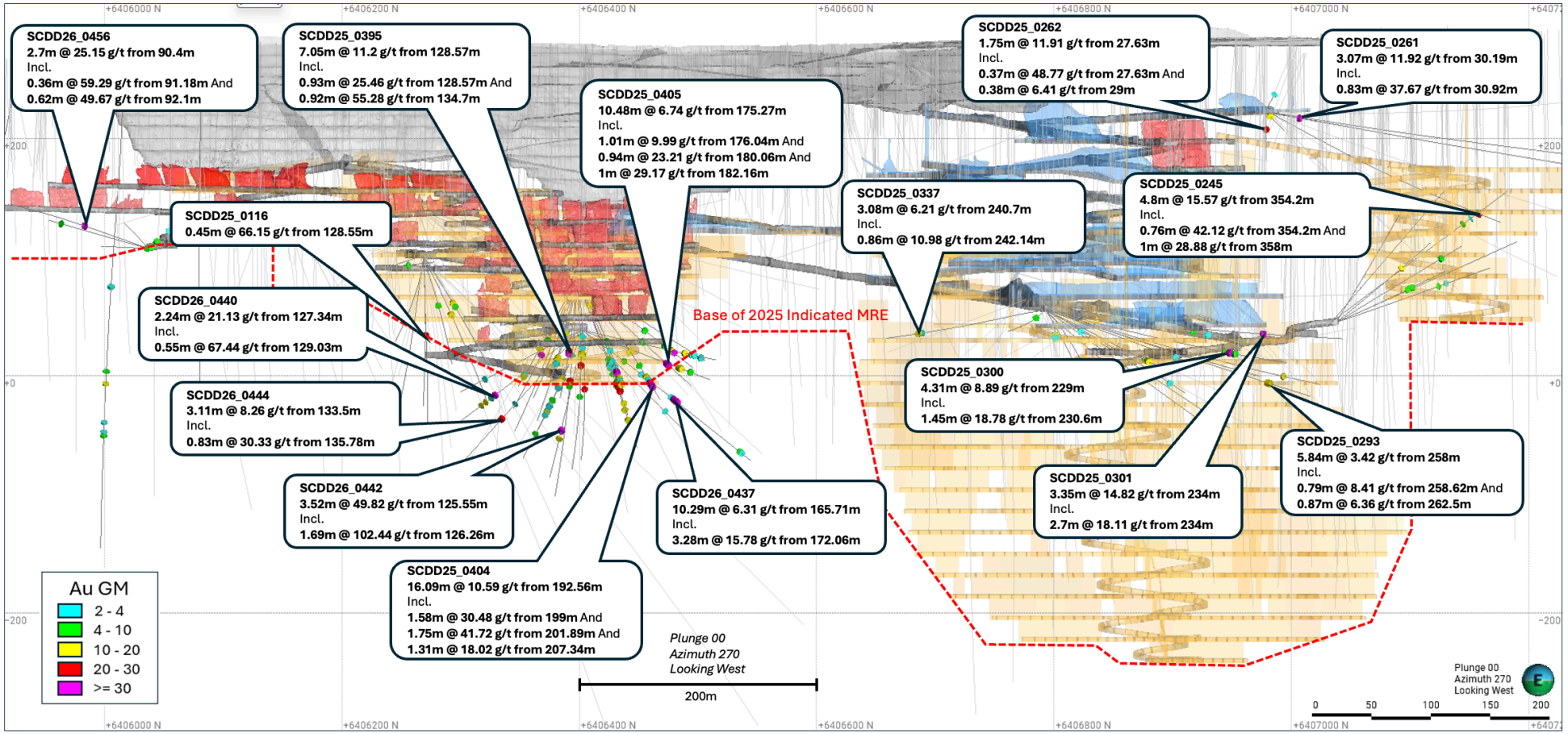

Figure: Scotia Underground Mine in long-section with recent drill results.

About the Scotia Mining Centre

The Scotia Mining Centre is located approximately 25 km south of Norseman and was discovered in 1893. The historic production recorded from the Scotia Mine via open pit and underground mining was 811,000 tonnes @ 5.9 g/t Au for 155,000 ounces. Scotia was actively mined from 1987 until 1996.

Pantoro Gold developed large-scale open pit mines at Scotia and Green Lantern in 2022, completing the current stage of open pit mining in October 2024. During that time, approximately 93,000 ounces were mined and processed from the open pits.

The Scotia Underground Mine development commenced in May 2024 and mining and development are ongoing. The current Scotia Underground Mine Mineral Resource is estimated at 1.90 Mt @ 5.32 g/t Au for 329,000 ounces. Refer to Appendix 3 for full details of the Scotia Mineral Resource and Ore Reserve.

The Scotia Underground Mine will be the largest underground mine at Norseman during the coming years and is a major focus for growth. Underground growth exploration drilling is planned to continue for the foreseeable future.

About the Norseman Gold Project

Pantoro Gold is focused on unlocking the full potential of its 100%-owned Norseman Gold Project.

The Project is located in the Eastern Goldfields of Western Australia, at the southern end of the highly productive Norseman-Wiluna greenstone belt and is one of the highest-grade goldfields within the Yilgarn Craton. The Project lies approximately 725 kilometres east of Perth and 200 kilometres south of Kalgoorlie.

Pantoro Gold has Ore Reserves which currently stand at 859,000 ounces. The company completed construction of a new 1.2 million tonnes per annum gold processing plant in 2022 and is undertaking production mining activities across its open pit and underground operations.

The current Total Mineral Resource is 4.6 million ounces of gold. Refer to Appendix 3 for full details of Pantoro Gold's Mineral Resource and Ore Reserve.

Many of the Mineral Resources defined to date remain open along strike and at depth, and in most cases the Mineral Resources have only been tested to shallow depths. In addition, there are numerous anomalies and mineralisation occurrences which are yet to be tested adequately to be placed into Mineral Resources, with several highly prospective targets already identified.

The Project comprises a number of near-contiguous mining tenements, most of which are pre-1994 Mining Leases.

The tenure includes approximately 70 lineal kilometres of the highly prospective Norseman-Wiluna greenstone belt covering approximately 800 square kilometres in total.

Historically, Norseman has produced more than 5.5 million ounces of gold since operations began in 1935. Pantoro Gold's growth strategy, as announced in June 2024, is centred on expanding its underground mining operations and scaling production at Norseman, initially targeting 100,000 ounces per annum and aiming to grow to over 200,000 ounces annually. With an active growth program and significant untapped potential, Pantoro Gold is poised for substantial growth in the coming years and expects to drill approximately 250,000 metres of combined RC, diamond and air core during FY2026.

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This announcement was authorised for release by Paul Cmrlec, Managing Director.

Appendix 1 – Table of Drill Results

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0106	6406270	386372	100	-15	93	266.8		190	190.3	0.3	1.28	0.19
SCDD25_0106	6406270	386372	100	-15	93	266.8		192.48	192.78	0.3	21.63	0.19
SCDD25_0109	6406269	386372	100	-19.6	83	275.05		103.31	103.72	0.41	1.4	0.29
SCDD25_0109	6406269	386372	100	-19.6	83	275.05		120.48	120.78	0.3	33.16	0.21
SCDD25_0110	6406270	386372	100	-20.4	75.9	270		105.5	108.65	3.15	3.71	2.24
SCDD25_0110	6406270	386372	100	-20.4	75.9	270		115	115.83	0.83	4.92	0.59
SCDD25_0110	6406270	386372	100	-20.4	75.9	270		118.75	119.23	0.48	1.95	0.34
SCDD25_0110	6406270	386372	100	-20.4	75.9	270		209	210	1	1.83	0.71
SCDD25_0112	6406269	386372	100	-25.3	89	297.5		159.7	160.45	0.75	1.76	0.58
SCDD25_0112	6406269	386372	100	-25.3	89	297.5		162.5	162.95	0.45	1.69	0.35
SCDD25_0112	6406269	386372	100	-25.3	89	297.5		273.45	274	0.55	1.32	0.42
SCDD25_0114	6406269	386372	100	-25.3	76	290		111.15	115.03	3.88	5.02	2.98
SCDD25_0114	6406269	386372	100	-25.3	76	290	Including	111.75	113.3	1.55	10.97	1.19
SCDD25_0114	6406269	386372	100	-25.3	76	290		121.36	124.4	3.04	0.78	2.34
SCDD25_0114	6406269	386372	100	-25.3	76	290		193.51	193.9	0.39	1.65	0.3
SCDD25_0115	6406269	386372	100	-26.5	94	329.8		234.55	234.87	0.32	4.41	0.25
SCDD25_0115	6406269	386372	100	-26.5	94	329.8		269.68	270	0.32	1.55	0.25
SCDD25_0115	6406269	386372	100	-26.5	94	329.8		292.4	292.8	0.4	1.05	0.31
SCDD25_0115	6406269	386372	100	-26.5	94	329.8		301	301.64	0.64	1.28	0.5
SCDD25_0116	6406269	386372	100	-30.4	88.8	302.8		124.8	125.5	0.7	1.29	0.58
SCDD25_0116	6406269	386372	100	-30.4	88.8	302.8		128.55	129	0.45	66.15	0.37
SCDD25_0116	6406269	386372	100	-30.4	88.8	302.8		170	171	1	1.09	0.82
SCDD25_0116	6406269	386372	100	-30.4	88.8	302.8		177.65	178	0.35	1	0.29
SCDD25_0116	6406269	386372	100	-30.4	88.8	302.8		231	231.4	0.4	4.46	0.33
SCDD25_0234	6406400	386370	80	-21.2	52	187.8		47.57	48.34	0.77	1.45	0.56
SCDD25_0234	6406400	386370	80	-21.2	52	187.8		111.52	112	0.48	1.13	0.35
SCDD25_0234	6406400	386370	80	-21.2	52	187.8		126	126.97	0.97	8.55	0.7
SCDD25_0234	6406400	386370	80	-21.2	52	187.8		179.4	181.9	2.5	1.45	1.8
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		109.1	110.4	1.3	1.98	1.13

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		127	130.05	3.05	0.67	2.66
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		146.14	151.3	5.16	4.66	4.5
SCDD25_0238	6406398	386370	80	-35.7	92	326.8	Including	146.14	146.51	0.37	23.47	0.32
SCDD25_0238	6406398	386370	80	-35.7	92	326.8	Including	147	147.35	0.35	35.1	0.31
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		155	156	1	5.06	0.87
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		201.75	202.05	0.3	1.35	0.26
SCDD25_0238	6406398	386370	80	-35.7	92	326.8		241.45	242.03	0.58	1.87	0.51
SCDD25_0245	6406982	386475	222	-14.5	298.1	392.9		354.2	359	4.8	15.57	3.91
SCDD25_0245	6406982	386475	222	-14.5	298.1	392.9	Including	354.2	354.96	0.76	42.12	0.62
SCDD25_0245	6406982	386475	222	-14.5	298.1	392.9	Including	358	359	1	28.88	0.81
SCDD25_0258	6406979	386481	222	-11	79	80.5		16	18.37	2.37	8.08	1.84
SCDD25_0258	6406979	386481	222	-11	79	80.5	Including	16.63	17.5	0.87	14.83	0.68
SCDD25_0259	6406979	386481	225	40.7	62	21		18.3	18.7	0.4	10	0.39
SCDD25_0261	6406979	386481	222	-9	30	80.4		30.19	33.26	3.07	11.92	2.32
SCDD25_0261	6406979	386481	222	-9	30	80.4	Including	30.92	31.75	0.83	37.67	0.63
SCDD25_0262	6406979	386481	222	-30	90	83.5		27.63	29.38	1.75	11.91	1.64
SCDD25_0262	6406979	386481	222	-30	90	83.5	Including	27.63	28	0.37	48.77	0.35
SCDD25_0262	6406979	386481	222	-30	90	83.5	Including	29	29.38	0.38	6.41	0.36
SCDD25_0262	6406979	386481	222	-30	90	83.5		43.18	43.52	0.34	1.65	0.32
SCDD25_0263B	6406238	386491	91	5.7	40.5	55		17.21	19.3	2.09	0.82	1.5
SCDD25_0263B	6406238	386491	91	5.7	40.5	55		24.2	25	0.8	7.65	0.57
SCDD25_0263B	6406238	386491	91	5.7	40.5	55		39.74	40.06	0.32	1.68	0.23
SCDD25_0264B	6406237	386492	91	9.9	60.0	50		15.75	16.05	0.3	1.99	0.23
SCDD25_0264B	6406237	386492	91	9.9	60.0	50		35.3	36	0.7	1.32	0.54
SCDD25_0292	6406795	386448	55	-13.5	35.8	299.7		257.5	259.85	2.35	7.76	1.89
SCDD25_0292	6406795	386448	55	-13.5	35.8	299.7	Including	259	259.85	0.85	11.89	0.68
SCDD25_0293	6406795	386448	55	-14.2	41	311.8		254.48	255.13	0.65	1.16	0.53
SCDD25_0293	6406795	386448	55	-14.2	41	311.8		258	263.84	5.84	3.42	4.74
SCDD25_0293	6406795	386448	55	-14.2	41	311.8	Including	258.62	259.41	0.79	8.41	0.64
SCDD25_0293	6406795	386448	55	-14.2	41	311.8	Including	262.5	263.37	0.87	6.36	0.71
SCDD25_0293	6406795	386448	55	-14.2	41	311.8		268.3	269.3	1	1.03	0.81

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0298	6406794	386450	55	-10.6	58	260.9		175	175.6	0.6	2.22	0.46
SCDD25_0298	6406794	386450	55	-10.6	58	260.9		220	221.15	1.15	1.98	0.89
SCDD25_0298	6406794	386450	55	-10.6	58	260.9		225.79	226.45	0.66	1.72	0.51
SCDD25_0299	6406794	386450	55	-10.8	66.6	280		182	183	1	1.06	0.77
SCDD25_0299	6406794	386450	55	-10.8	66.6	280		225	226	1	3.52	0.77
SCDD25_0299	6406794	386450	55	-10.8	66.6	280		229.1	236.7	7.6	2.27	5.89
SCDD25_0299	6406794	386450	55	-10.8	66.6	280	Including	230.5	231.75	1.25	5.64	0.97
SCDD25_0300	6406794	386450	55	-10.4	45	305.9		192.91	193.21	0.3	3.02	0.23
SCDD25_0300	6406794	386450	55	-10.4	45	305.9		224.19	224.72	0.53	9.42	0.41
SCDD25_0300	6406794	386450	55	-10.4	45	305.9		229	233.31	4.31	8.89	3.32
SCDD25_0300	6406794	386450	55	-10.4	45	305.9	Including	230.6	232.05	1.45	18.78	1.12
SCDD25_0300	6406794	386450	55	-10.4	45	305.9		236.15	240.5	4.35	2.53	3.35
SCDD25_0300	6406794	386450	55	-10.4	45	305.9		253.79	254.3	0.51	3.45	0.39
SCDD25_0301	6406795	386449	55	-6.2	37	327		234	237.35	3.35	14.82	2.42
SCDD25_0301	6406795	386449	55	-6.2	37	327	Including	234	236.7	2.7	18.11	1.95
SCDD25_0302	6406794	386450	55	-6	52	233.45		143.51	144	0.49	1.1	0.35
SCDD25_0302	6406794	386450	55	-6	52	233.45		209.06	209.86	0.8	9.39	0.58
SCDD25_0302	6406794	386450	55	-6	52	233.45		226.67	226.97	0.3	3.33	0.22
SCDD25_0302	6406794	386450	55	-6	52	233.45		232.03	233.45	1.42	1.55	1.02
SCDD25_0303	6406794	386450	56	-5.8	60	274.7		211.6	211.9	0.3	3.1	0.22
SCDD25_0303	6406794	386450	56	-5.8	60	274.7		223	224	1	1.12	0.72
SCDD25_0305	6406794	386450	55	-20	55.1	293.7		252.63	252.93	0.3	1.72	0.26
SCDD25_0307	6406793	386450	56	-5.9	79	245		186	188	2	1.69	1.44
SCDD25_0308	6406793	386450	56	-5.1	86	249.5		222	227	5	3.34	3.54
SCDD25_0308	6406793	386450	56	-5.1	86	249.5	Including	223	224	1	10.34	0.71
SCDD25_0308	6406793	386450	56	-5.1	86	249.5		240.2	241.5	1.3	3.35	0.92
SCDD25_0308	6406793	386450	56	-5.1	86	249.5		245	246	1	4.04	0.71
SCDD25_0309	6406793	386450	55	-14.7	61	270		121	121.5	0.5	1	0.41
SCDD25_0309	6406793	386450	55	-14.7	61	270		237	238	1	3.78	0.82
SCDD25_0309	6406793	386450	55	-14.7	61	270		259.6	262	2.4	0.82	1.96
SCDD25_0310	6406793	386450	55	-19.4	70	266.6		59.01	60	0.99	1.05	0.85

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SCDD25_0310	6406793	386450	55	-19.4	70	266.6		79.68	80.14	0.46	1.52	0.4
SCDD25_0310	6406793	386450	55	-19.4	70	266.6		188	188.3	0.3	1.52	0.26
SCDD25_0311	6406793	386450	55	-14.9	80	259.2		241	242	1	1.09	0.82
SCDD25_0313	6406792	386450	56	-4.3	95	246.2		75.3	75.6	0.3	13.41	0.21
SCDD25_0313	6406792	386450	56	-4.3	95	246.2		228.25	228.55	0.3	1.14	0.21
SCDD25_0313	6406792	386450	56	-4.3	95	246.2		230.85	232	1.15	1.46	0.8
SCDD25_0319	6406894	386529	145	8.5	68.6	85.8		53.8	55	1.2	2.97	0.9
SCDD25_0319	6406894	386529	145	8.5	68.6	85.8		58	59	1	1.49	0.75
SCDD25_0319	6406894	386529	145	8.5	68.6	85.8		63	64	1	1.05	0.75
SCDD25_0319	6406894	386529	145	8.5	68.6	85.8		67.4	68.87	1.47	1.77	1.1
SCDD25_0323	6406894	386529	144	-3.5	40.7	98.4		73	74	1	17.67	0.69
SCDD25_0323	6406894	386529	144	-3.5	40.7	98.4		79.76	80.24	0.48	1.05	0.33
SCDD25_0323	6406894	386529	144	-3.5	40.7	98.4		89.95	90.25	0.3	1.31	0.21
SCDD25_0324	6406894	386529	143	-27.1	94.1	90.9		56	57	1	2.2	0.92
SCDD25_0324	6406894	386529	143	-27.1	94.1	90.9		63.5	66.42	2.92	2.89	2.69
SCDD25_0324	6406894	386529	143	-27.1	94.1	90.9		82.7	83	0.3	6.38	0.28
SCDD25_0337	6406791	386450	55	-3.6	115	300.15		111.88	112.67	0.79	2.24	0.55
SCDD25_0337	6406791	386450	55	-3.6	115	300.15		121.5	122.18	0.68	1.05	0.47
SCDD25_0337	6406791	386450	55	-3.6	115	300.15		223.8	224.1	0.3	1.49	0.21
SCDD25_0337	6406791	386450	55	-3.6	115	300.15		235	236	1	3.23	0.69
SCDD25_0337	6406791	386450	55	-3.6	115	300.15		240.7	243.78	3.08	6.21	2.13
SCDD25_0337	6406791	386450	55	-3.6	115	300.15	Including	242.14	243	0.86	10.98	0.59
SCDD25_0389	6406397	386370	80	-24.4	104	209.3		133	135	2	5.42	1.52
SCDD25_0389	6406397	386370	80	-24.4	104	209.3		182	183	1	1.15	0.76
SCDD25_0389	6406397	386370	80	-24.4	104	209.3		185.31	186.05	0.74	2.88	0.56
SCDD25_0389	6406397	386370	80	-24.4	104	209.3		188.6	189.91	1.31	11.24	0.99
SCDD25_0390	6406397	386370	80	-28.2	104	225		106	107	1	7.54	0.8
SCDD25_0390	6406397	386370	80	-28.2	104	225		130.95	133.43	2.48	15.43	1.98
SCDD25_0390	6406397	386370	80	-28.2	104	225	Including	131.88	133.43	1.55	23.69	1.24
SCDD25_0390	6406397	386370	80	-28.2	104	225		154.47	154.94	0.47	3.57	0.38

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0390	6406397	386370	80	-28.2	104	225		192.66	192.97	0.31	5.18	0.25
SCDD25_0391	6406397	386370	80	-31.6	102.8	238.2		41.39	41.69	0.3	3.17	0.25
SCDD25_0391	6406397	386370	80	-31.6	102.8	238.2		156.3	156.7	0.4	2.99	0.33
SCDD25_0392	6406397	386370	80	-27.3	98.1	216.6		96.45	98.88	2.43	0.41	1.92
SCDD25_0392	6406397	386370	80	-27.3	98.1	216.6		124.01	124.54	0.53	1.81	0.42
SCDD25_0392	6406397	386370	80	-27.3	98.1	216.6		170	170.3	0.3	1.15	0.24
SCDD25_0392	6406397	386370	80	-27.3	98.1	216.6		183	183.3	0.3	3.2	0.24
SCDD25_0392	6406397	386370	80	-27.3	98.1	216.6		187.94	188.26	0.32	3.56	0.25
SCDD25_0393	6406397	386370	80	-30.8	97	231.5		130.59	131.19	0.6	11.38	0.5
SCDD25_0393	6406397	386370	80	-30.8	97	231.5		136	136.3	0.3	2.28	0.25
SCDD25_0393	6406397	386370	80	-30.8	97	231.5		139.55	140.2	0.65	1.68	0.54
SCDD25_0394	6406397	386370	80	-21.8	93	204.1		119.09	119.49	0.4	35.92	0.29
SCDD25_0394	6406397	386370	80	-21.8	93	204.1		130.2	131	0.8	1.27	0.58
SCDD25_0394	6406397	386370	80	-21.8	93	204.1		140	140.55	0.55	1.45	0.4
SCDD25_0394	6406397	386370	80	-21.8	93	204.1		174.26	183	8.74	3.63	6.37
SCDD25_0394	6406397	386370	80	-21.8	93	204.1	Including	174.26	174.59	0.33	21.31	0.24
SCDD25_0394	6406397	386370	80	-21.8	93	204.1	Including	176.64	176.94	0.3	18.05	0.22
SCDD25_0394	6406397	386370	80	-21.8	93	204.1	Including	179.55	179.93	0.38	10.06	0.28
SCDD25_0394	6406397	386370	80	-21.8	93	204.1	Including	182.57	183	0.43	15.99	0.31
SCDD25_0394	6406397	386370	80	-21.8	93	204.1		187.47	189.55	2.08	1.47	1.52
SCDD25_0395	6406398	386370	80	-27.1	92	216.4		128.57	135.62	7.05	11.2	5.56
SCDD25_0395	6406398	386370	80	-27.1	92	216.4	Including	128.57	129.5	0.93	25.46	0.73
SCDD25_0395	6406398	386370	80	-27.1	92	216.4	Including	134.7	135.62	0.92	55.28	0.73
SCDD25_0395	6406398	386370	80	-27.1	92	216.4		189	190	1	1.42	0.79
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		47	47.65	0.65	1.02	0.47
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		79.7	80.75	1.05	1.42	0.76
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		130.17	130.65	0.48	8.28	0.35
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		141.62	142.35	0.73	1.33	0.53
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		152.2	153	0.8	1.08	0.58
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		157	159.57	2.57	1.33	1.86

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		163.9	164.9	1	1.38	0.72
SCDD25_0396	6406398	386370	80	-21.3	85	192.4		169	178	9	3.56	6.5
SCDD25_0396	6406398	386370	80	-21.3	85	192.4	Including	176.47	178	1.53	12.24	1.11
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		50.3	51.38	1.08	1.48	0.89
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		93	94	1	7.02	0.82
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		108.42	108.9	0.48	2.33	0.39
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		132.05	132.7	0.65	2.94	0.53
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		139.7	142.9	3.2	7.2	2.63
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7	Including	139.7	140	0.3	57.9	0.25
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		153.9	156.42	2.52	0.88	2.07
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		188.85	189.25	0.4	1.09	0.33
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		193.6	194.1	0.5	10.93	0.41
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		197	197.45	0.45	1.45	0.37
SCDD25_0398	6406398	386370	80	-30.3	86.5	320.7		304.9	305.2	0.3	1.66	0.25
SCDD25_0399	6406398	386370	80	-21.3	77	207.6		55.2	56.55	1.35	7.92	0.98
SCDD25_0399	6406398	386370	80	-21.3	77	207.6		139.5	147	7.5	1.01	5.42
SCDD25_0399	6406398	386370	80	-21.3	77	207.6		160.6	161.9	1.3	1.73	0.94
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		46.25	46.55	0.3	1.34	0.24
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		87.56	88.17	0.61	1.57	0.48
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		156.5	157.22	0.72	3.69	0.56
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		165.73	170	4.27	1.21	3.35
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		175.46	183	7.54	5.46	5.91
SCDD25_0400	6406398	386370	80	-26.6	76	219.6	Including	181.3	182.26	0.96	13.15	0.75
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		188.89	193.8	4.91	2.76	3.85
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		196	197	1	3.57	0.78
SCDD25_0400	6406398	386370	80	-26.6	76	219.6		200.99	205.67	4.68	2.89	3.67
SCDD25_0400	6406398	386370	80	-26.6	76	219.6	Including	200.99	202	1.01	9.72	0.79
SCDD25_0401	6406398	386370	80	-31	75	236.2		129.96	130.26	0.3	2.15	0.25
SCDD25_0401	6406398	386370	80	-31	75	236.2		133.7	134	0.3	30.41	0.25
SCDD25_0401	6406398	386370	80	-31	75	236.2		138.5	138.8	0.3	32.03	0.25

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0401	6406398	386370	80	-31	75	236.2		141.5	143.5	2	1.3	1.66
SCDD25_0401	6406398	386370	80	-31	75	236.2		173.87	185.3	11.43	3.18	9.47
SCDD25_0401	6406398	386370	80	-31	75	236.2	Including	173.87	174.87	1	7.59	0.83
SCDD25_0401	6406398	386370	80	-31	75	236.2	Including	184.3	185.3	1	8.94	0.83
SCDD25_0401	6406398	386370	80	-31	75	236.2		189.28	192.24	2.96	7.87	2.45
SCDD25_0401	6406398	386370	80	-31	75	236.2	Including	191.17	191.8	0.63	25.53	0.52
SCDD25_0401	6406398	386370	80	-31	75	236.2		212.62	213.97	1.35	7.79	1.12
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4		128.04	129.5	1.46	4.04	1.03
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4		168.25	171.65	3.4	1.34	2.39
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4		179.84	185.3	5.46	3.22	3.84
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4	Including	179.84	180.84	1	9.22	0.7
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4	Including	181.38	182.26	0.88	6.2	0.62
SCDD25_0402	6406396	386370	80	-19.7	59.3	231.4		188.37	189.55	1.18	26.78	0.83
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		138.45	138.8	0.35	29.33	0.27
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		148	149	1	1.21	0.78
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		165.41	166.38	0.97	6.28	0.75
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		170	170.5	0.5	3.95	0.39
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		186	190.3	4.3	2.87	3.33
SCDD25_0404	6406398	386370	80	-25.8	66.6	232	Including	187.92	189.5	1.58	6.62	1.22
SCDD25_0404	6406398	386370	80	-25.8	66.6	232		192.56	208.65	16.09	10.59	12.47
SCDD25_0404	6406398	386370	80	-25.8	66.6	232	Including	199	200.58	1.58	30.48	1.22
SCDD25_0404	6406398	386370	80	-25.8	66.6	232	Including	201.89	203.64	1.75	41.72	1.36
SCDD25_0404	6406398	386370	80	-25.8	66.6	232	Including	207.34	208.65	1.31	18.02	1.02
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8		63.96	64.29	0.33	3.53	0.25
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8		91.87	92.17	0.3	1.01	0.23
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8		126.63	130	3.37	1.67	2.58
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8		175.27	185.75	10.48	6.74	8.01
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8	Including	176.04	177.05	1.01	9.99	0.77
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8	Including	180.06	181	0.94	23.21	0.72
SCDD25_0405	6406398	386370	80	-24.9	60.3	230.8	Including	182.16	183.16	1	29.17	0.76

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		122.1	123.5	1.4	1.54	1.23
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		127	128	1	2.85	0.88
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		135.75	136.12	0.37	12.54	0.32
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		154.3	155.5	1.2	8.48	1.05
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		191.43	192.69	1.26	8.34	1.11
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		206.82	209.77	2.95	4.42	2.59
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		213.3	213.63	0.33	3.43	0.29
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		218	224.2	6.2	1.7	5.44
SCDD25_0408	6406398	386370	80	-36.4	72.7	252.5		227.56	227.86	0.3	1.48	0.26
SCDD26_0427	6407039	386403	47	36.6	63.1	152.3		127.03	128.2	1.17	1.61	1.14
SCDD26_0428	6407038	386402	46	24.2	57.5	167.6		112.61	114	1.39	14.21	1.25
SCDD26_0429	6407039	386402	45	14.3	54.2	167.8		106.55	107	0.45	16.04	0.37
SCDD26_0429	6407039	386402	45	14.3	54.2	167.8		110.46	110.76	0.3	14.31	0.24
SCDD26_0429	6407039	386402	45	14.3	54.2	167.8		114.24	115.3	1.06	4.83	0.86
SCDD26_0431	6407039	386402	46	23.6	45.6	167.6		122.17	122.61	0.44	2.89	0.39
SCDD26_0431	6407039	386402	46	23.6	45.6	167.6		138	140	2	4.96	1.79
SCDD26_0432	6407039	386402	45	14.1	41.9	182.6		119.26	119.7	0.44	12.34	0.36
SCDD26_0432	6407039	386402	45	14.1	41.9	182.6		128.56	129	0.44	7.59	0.36
SCDD26_0433	6407034	386403	45	34.2	24.3	200.3		148.37	150.3	1.93	2.73	1.86
SCDD26_0433	6407034	386403	45	34.2	24.3	200.3		157.87	158.17	0.3	10.06	0.29
SCDD26_0433	6407034	386403	45	34.2	24.3	200.3		166.64	167.12	0.48	4.47	0.46
SCDD26_0435	6406403	386385	38	-8.2	52.6	198.1		67.7	68	0.3	2.45	0.16
SCDD26_0435	6406403	386385	38	-8.2	52.6	198.1		147.43	149.9	2.47	5.83	1.35
SCDD26_0435	6406403	386385	38	-8.2	52.6	198.1	Including	147.83	148.41	0.58	20.44	0.32
SCDD26_0435	6406403	386385	38	-8.2	52.6	198.1		158.4	160.3	1.9	2.03	1.04
SCDD26_0435	6406403	386385	38	-8.2	52.6	198.1		163	164.63	1.63	1.91	0.89
SCDD26_0436	6406403	386385	38	-13.6	54	199.6		146.67	153.25	6.58	2.12	4.11
SCDD26_0436	6406403	386385	38	-13.6	54	199.6	Including	150.15	150.9	0.75	5.37	0.47
SCDD26_0436	6406403	386385	38	-13.6	54	199.6		166	167.39	1.39	5.12	0.87
SCDD26_0436	6406403	386385	38	-13.6	54	199.6		180.05	180.35	0.3	1.29	0.19
SCDD26_0437	6406403	386385	38	-21.2	59	330		73	74	1	4.19	0.72

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD26_0437	6406403	386385	38	-21.2	59	330		105	106	1	3.97	0.72
SCDD26_0437	6406403	386385	38	-21.2	59	330		135.07	136	0.93	1.15	0.67
SCDD26_0437	6406403	386385	38	-21.2	59	330		160.92	161.22	0.3	10.81	0.22
SCDD26_0437	6406403	386385	38	-21.2	59	330		165.71	176	10.29	6.31	7.42
SCDD26_0437	6406403	386385	38	-21.2	59	330	Including	172.06	175.34	3.28	15.78	2.37
SCDD26_0437	6406403	386385	38	-21.2	59	330		304.39	305.08	0.69	7.05	0.5
SCDD26_0437	6406403	386385	38	-21.2	59	330		309.1	309.38	0.28	9.72	0.2
SCDD26_0438	6406403	386385	38	-25.8	60	216.4		162.07	162.45	0.38	5.81	0.29
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		77.63	78.05	0.42	4.52	0.35
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		84	84.31	0.31	1.18	0.26
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		87.19	87.49	0.3	59.54	0.25
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		90.7	93	2.3	1.32	1.92
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		112.68	113.6	0.92	11.28	0.77
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		119.94	122.8	2.86	1.35	2.39
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		128.5	128.86	0.36	7.3	0.3
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		131.75	132.4	0.65	21.39	0.54
SCDD26_0439	6406403	386385	38	-31.7	105	171.4		168.12	168.7	0.58	12.49	0.48
SCDD26_0440	6406401	386385	38	-25.3	128	180		127.34	129.58	2.24	21.13	1.72
SCDD26_0440	6406401	386385	38	-25.3	128	180	Including	129.03	129.58	0.55	67.44	0.42
SCDD26_0440	6406401	386385	38	-25.3	128	180		133.9	134.9	1	3.56	0.77
SCDD26_0440	6406401	386385	38	-25.3	128	180		142.3	143	0.7	24.63	0.54
SCDD26_0440	6406401	386385	38	-25.3	128	180		149.18	149.6	0.42	30.06	0.32
SCDD26_0441	6406401	386385	38	-17.3	127.8	173.6		136.96	138	1.04	3.34	0.7
SCDD26_0442	6406403	386385	38	-41.6	100	190		115.75	116	0.25	3.4	0.23
SCDD26_0442	6406403	386385	38	-41.6	100	190		125.55	129.07	3.52	49.82	3.23
SCDD26_0442	6406403	386385	38	-41.6	100	190	Including	126.26	127.95	1.69	102.44	1.55
SCDD26_0442	6406403	386385	38	-41.6	100	190		137.3	138.8	1.5	10.23	1.38
SCDD26_0444	6406401	386385	38	-33.8	126.5	205		101.61	101.98	0.37	1.73	0.32
SCDD26_0444	6406401	386385	38	-33.8	126.5	205		111.5	112.25	0.75	3.68	0.64
SCDD26_0444	6406401	386385	38	-33.8	126.5	205		133.5	136.61	3.11	8.26	2.66
SCDD26_0444	6406401	386385	38	-33.8	126.5	205	Including	135.78	136.61	0.83	30.33	0.71

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCDD26_0444	6406401	386385	38	-33.8	126.5	205		140.73	141.21	0.48	1.46	0.41
SCDD26_0445	6406403	386385	38	-29	88	237.6		84.35	84.8	0.45	1.2	0.36
SCDD26_0445	6406403	386385	38	-29	88	237.6		89.35	89.75	0.4	4.68	0.32
SCDD26_0445	6406403	386385	38	-29	88	237.6		92.79	93.3	0.51	1.75	0.41
SCDD26_0445	6406403	386385	38	-29	88	237.6		103.48	104.38	0.9	27.72	0.73
SCDD26_0445	6406403	386385	38	-29	88	237.6		116.4	116.7	0.3	1.33	0.24
SCDD26_0445	6406403	386385	38	-29	88	237.6		124.67	124.97	0.3	1.23	0.24
SCDD26_0445	6406403	386385	38	-29	88	237.6		131.47	131.88	0.41	1.07	0.33
SCDD26_0445	6406403	386385	38	-29	88	237.6		136.66	137.48	0.82	2.21	0.66
SCDD26_0445	6406403	386385	38	-29	88	237.6		162.4	162.7	0.3	2.29	0.24
SCDD26_0446	6406403	386385	38	-27.8	101.7	234.5		86.37	86.8	0.43	32.99	0.34
SCDD26_0446	6406403	386385	38	-27.8	101.7	234.5		125.27	125.57	0.3	25.31	0.24
SCDD26_0446	6406403	386385	38	-27.8	101.7	234.5		153.01	154	0.99	2.07	0.79
SCDD26_0448	6406037	386609	107	18.9	67.5	74		18.51	20.11	1.6	4.67	1.37
SCDD26_0448	6406037	386609	107	18.9	67.5	74		48.32	48.62	0.3	10.99	0.26
SCDD26_0448	6406037	386609	107	18.9	67.5	74		50.77	51.7	0.93	1.09	0.8
SCDD26_0448	6406037	386609	107	18.9	67.5	74		55.46	55.76	0.3	2.24	0.26
SCDD26_0451	6406037	386609	107	2.4	86.3	66.6		54	54.4	0.4	12.47	0.27
SCDD26_0452	6406037	386609	107	17.3	106.5	76.3		22	22.3	0.3	3.32	0.25
SCDD26_0455	6406037	386609	107	2.3	117	90		3	3.3	0.3	15.52	0.2
SCDD26_0455	6406037	386609	107	2.3	117	90		80.75	81.39	0.64	2	0.43
SCDD26_0456	6406037	386609	107	12.4	127	195		90.4	93.1	2.7	25.15	2.14
SCDD26_0456	6406037	386609	107	12.4	127	195	Including	91.18	91.54	0.36	59.29	0.29
SCDD26_0456	6406037	386609	107	12.4	127	195	Including	92.1	92.72	0.62	49.67	0.49
SCDD26_0458	6406037	386609	107	11	133	125.9		109.57	110.46	0.89	10.32	0.69
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		229.91	232.49	2.58	1.43	2.57
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		317	317.96	0.96	9.88	0.96
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		329.49	331	1.51	7.52	1.5
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		355.6	356	0.4	3.6	0.4
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		366	366.88	0.88	1.09	0.88
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		369	371	2	1.92	1.99

Hole_ID	Northing	Easting	RL	Dip (Degrees)	Azimuth (Degrees)	End of Hole Depth (m)	Comments	Downhole From (m)	Downhole To (m)	Downhole Intersection (m)	Au gpt	Est. True Width (m)
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		374.72	375.09	0.37	1.07	0.37
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		379	380	1	2.7	1
SCRCD25_268	6406015	386879	271	-59.5	271.1	500		382.9	384.39	1.49	2.73	1.48
SCRCD25_271	6405932	386795	270	-60.5	252.4	270.3		187.8	188.82	1.02	5.38	1.02
SCRCD25_271	6405932	386795	270	-60.5	252.4	270.3		234.76	235.14	0.38	12.18	0.38
SCRCD25_272	6405945	386836	269	-61.3	268.3	370		185	186	1	1.62	1
SCRCD25_272	6405945	386836	269	-61.3	268.3	370		225.28	226	0.72	15.53	0.72
SCRCD25_272	6405945	386836	269	-61.3	268.3	370		240.18	241.2	1.02	3.42	1.02
SCRCD25_273	6405946	386838	269	-60.6	252.8	366.4		194	195.5	1.5	1.32	1.5
SCRCD25_273	6405946	386838	269	-60.6	252.8	366.4		206.4	207.4	1	1.41	1
SCRCD25_273	6405946	386838	269	-60.6	252.8	366.4		277	280	3	8.68	2.99
SCRCD25_273	6405946	386838	269	-60.6	252.8	366.4	Including	277	278.1	1.1	21.69	1.1
SCRCD25_273	6405946	386838	269	-60.6	252.8	366.4		287.8	288.1	0.3	29.29	0.3
SCRCD25_274	6406081	386760	275	-59.6	269.6	330.4		202	202.5	0.5	1.56	0.5
SCDD25_0248	6406982	386475	222	-6.1	306.7	453.2	NSI					
SCDD25_0249	6406982	386475	222	-5.4	313.5	494.1	NSI					
SCDD25_0297	6406794	386450	55	-10.5	52	314.5	NSI					
SCDD25_0306	6406794	386450	55	-20	59	320	NSI					
SCDD25_0314	6406793	386450	55	-10.6	80	255.2	NSI					
SCDD26_0430	6407034	386403	45	40.5	40.8	170.4	NSI					
SCDD26_0434	6407039	386402	46	20.9	31.6	194.5	NSI					

NSI: No significant intersection.

Appendix 2 – JORC Code 2012 Edition – Table 1

Section 1: Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. • Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. • Aspects of the determination of mineralisation that are Material to the Public Report. • In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	• This release reports assay results from underground grade control and extensional diamond drilling, in addition to surface RC drilling with diamond tails, undertaken to infill and expand the current Mineral Resource at the Scotia underground mine. • The diamond drill core sampled is NQ2. • All core is logged and sampled according to geology, with only selected samples assayed. Core is halved, using an Almonte core saw. The right-hand side (down hole) side of core is assayed, with the left side half containing orientation lines retained in core trays on site for further analysis. Samples are a maximum of 1.2m, with shorter intervals utilised according to geology. • Core is aligned, measured and marked in metre intervals referenced back to downhole core blocks. • Diamond drilling is completed to industry standard and sample intervals (0.3m-1.2m) are selected based on geological criteria. • For RC samples, a Metzke fixed cone splitter is used, with double chutes for field duplicates, Infinite adjustment between 4 – 15% per sample chute sampled every 1m. • **Diamond Core Samples** - 0.5-3kg samples are currently submitted to the onsite Intertek primary assay facility in Norseman, WA in preparation for photon assay analysis. Prior to May 2025, samples were dispatched to the external accredited laboratory (Bureau Veritas (BVA) Kalgoorlie) where they were crushed (<10mm) and pulverised to a pulp (P90 75 µm) in preparation for fire assay (40g charge). • Where visible gold is encountered and observed during logging, Screen Fire Assays are conducted when appropriate. Blanks (bricks) are routinely run through the core saw after observations of visible gold. Feldspar flushes are routinely run through crushers after samples containing visible gold and assayed to determine potential contamination. • **RC Samples** – 2-7kg samples are currently submitted to the onsite Intertek primary assay facility in Norseman, WA in preparation for photon assay analysis. Prior to May 2025, samples were dispatched to an external accredited laboratory where they (<10mm) and pulverised to a pulp (P90 75 µm) in preparation for fire assay (40g charge).

Criteria	JORC Code explanation	Commentary
Sampling techniques (continued)		• **Historic RC Drilling** - RC drilling was used to obtain 1 m samples from which 2-3 kg split via a splitter attached to the cyclone assembly of the drill rig. From the commencement of the mine until late 1995 the assaying was done on site until the closure of the onsite laboratory the samples were sent to Silver Lake lab at Kambalda. From November 2001 the samples were sent to Analabs in Kalgoorlie, subsequently owned and operated by the SGS group. The samples have always been fire assayed with various charge weights (generally either 30 or 50g). The method was (using the SGS codes) DRY11 (sample drying, 105°C), CRU24 (crush > 3.5kg, various mesh sizes per kg), SPL26 (riffle splitting, per kg), PUL48 (pulv, Cr Steel, 75µm, 1.5 to 3kg), FAA505 (AU FAS, AAS, 50g) (two of these were performed), and WST01 (waste disposal). • At Analabs the total sample was dried and milled in an LM5 mill to a nominal 90% passing -75µm. An analytical pulp of approximately 200g was sub sampled from the bulk and the milled residue was retained for future reference. All the preparation equipment was flushed with barren feldspar prior to the commencement of the job. A 50 gram sample was fused in a lead collection fire assay. The resultant prill is dissolved in aqua regia and the gold content of the sample is determined by AAS. For samples that contained visible free gold the screen fire assay method was used. It involved a 1000g sample screened through a 106µm mesh. The resulting plus and minus fractions were then analysed for gold by fire assay. Information reported included size fraction weight, coarse and fine fraction gold content and calculated gold.
Drilling techniques	• Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	• Underground diamond drilling is completed utilising NQ2 (standard tube). • Core is oriented routinely utilising an Axis Champ orientation device. • Historic Underground drilling was completed using electric hydraulic drill rigs with standard core LTK46 and LTK48 both with the same nominal core size of 38mm. • RC – Reverse circulation drilling was carried out using a face sampling hammer and a 5&5/8 inch diameter bit • Surface DD – HQ and NQ2 diamond tail completed on RC or Rock Roller pre-collars. All core has orientations lines marked where possible, with confidence and quality marked accordingly.

Criteria	JORC Code explanation	Commentary
Drill sample recovery	• Method of recording and assessing core and chip sample recoveries and results assessed. • Measures taken to maximise sample recovery and ensure representative nature of the samples. • Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	• All holes were logged onsite by an experienced geologist. Recovery and sample quality were visually observed and recorded. • Diamond drilling practices result in high recovery in competent ground as part of the current drill program. • No significant core loss has been noted in fresh material. Good core recovery has generally been achieved in all sample types in the current drilling program. Core recovery and core loss is recorded by drillers on core blocks and verified during core measuring and mark up. Core loss is recorded and logged. • RC sample recoveries are monitored by visual inspection of split reject, and lab weight samples are recorded and reviewed. • RC drilling by previous operators is considered to have been to industry standard for the time. • Historic holes have been inspected and core in the ore zones appears competent, with no evidence of core loss.
Logging	• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged.	• Geological logging is completed by a qualified geologist and logging parameters include: depth from, depth to, condition, weathering, oxidation, lithology, texture, colour, alteration style, alteration intensity, alteration mineralogy, sulphide content and composition, quartz content, veining, and general comments. • Logging is quantitative and qualitative with all core photographed wet. • All RC samples are chip trayed with each chip tray being photographed. • 100% of the relevant intersections are logged. • Paper logs of historic drill holes have been cross checked to database as part of the validation.
Sub-sampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• As of May 2025, Scotia drill core preparation and analysis is performed by Intertek at their analysis facility in Maddington, Perth, WA in preparation for photon assay. From September 2025, an onsite photon assay facility was also utitlised for analysis. Using a robotic shuttle, high energy x-rays are then fired at the sample causing excitation of atomic nuclei allowing detection of gold content. • Sample preparation for photon assay involves drying the sample at 105 degrees celsius for 12 hours, followed by crushing the sample to 85% passing 3 mm using either an Orbis 100 or Orbis 50 crusher. A ~500g sample jar is then filled for analysis. • For photon assay, fill checks are carried out for every sample to determine the jar fill rate, which is an 80% minimum fill per sample. Any sample that falls below this threshold is sent back to the sample preparation stage. The jar fill rate is used for density and volume calculations as part of the final reported gold value.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation (continued)		• Prior to May 2025, sample preparation and assaying of Scotia drill core and RC samples using fire assay was performed at BVA at their laboratory in Kalgoorlie, WA. • For fire assay samples, coarse grind checks at the crushing stage (3 mm) were carried out at a ratio of 1:25 samples with 90% of the sample volume reporting through the sieve required for a pass. Pulp grind checks at the pulverizing stage (75 µm) were carried out at a ratio of 1:25 samples with 90% of the sample volume reporting through the sieve required for a pass. • Core samples are sawn in half utilising an Almonte core-saw, with one half used for assaying and the other half retained in core trays on site for future analysis. • For core samples, core is separated into sample intervals and separately bagged for analysis at the certified laboratory. Core was cut under the supervision of an experienced geologist, was routinely cut to the right of the orientation line. Where no orientation line is present the core is cut on the apex of the dominant vein or structural feature. • All mineralised zones are sampled as well as material considered barren either side of the mineralised interval. • Field duplicates i.e. other half of core or ¼ core have not been routinely collected. • Half core is considered appropriate for diamond drill samples. • RC samples are taken off the fixed cone splitter, generally dry. • Field duplicates for RC drilling are routinely collected • RC drilling and sampling practices by previous operators are considered to have been conducted to industry standard for the time. • Visual inspection of the ~70% of historic holes which have been half cored and sampled either side of ore zones to define waste boundary.

Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	• The assay methods used, including fire assay with 40g charge approach total mineral consumption and are typical of industry standard practice. Photon assay offers improved measurement precision, simplified sample preparation and elimination of pulverisation. The technique is considered total and appropriate for the style of mineralisation under consideration. The increased size of photon assay sample is considered adequate to compensate for the larger particle size of the sample given the nature of mineralization being measured. • Standards are inserted at a ratio of 1:20. The results are reviewed on a per-batch basis and batches of samples are re-analysed if the result is greater than three standard deviations from the expected result. Any result outside of two standard deviations is flagged for investigation by a geologist and may also be re-assayed. QAQC results are reviewed on monthly and longer timeframes. • Blanks are inserted into the sample sequence at a ratio of 1:50, except where high grade mineralisation is expected. In these cases, a Blank is inserted after the high grade sample to test for contamination. Results greater than 0.2 g/t are investigated, and re-assayed if appropriate. • A range of Certified Reference materials (CRM') are selected to cover the wide range of grades in the deposits. CRM's used are appropriate and certified for the analysis types undertaken. • Lab standards and repeats are included as part of the QAQC system. In addition, the laboratory has its own internal QAQC comprising standards, blanks and duplicates. • Follow-up re-assaying is performed by the laboratory upon company request following review of assay data. Acceptable bias and precision is noted in results given the nature of the deposit and the level of classification. • In relation to the historic assay results it is assumed the procedures adopted at the WMC laboratory in Kalgoorlie and subsequently Analabs post June 1996 were to industry standard for the time.
Verification of sampling and assaying	• The verification of significant intersections by either independent or alternative company personnel. • The use of twinned holes. • Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. • Discuss any adjustment to assay data.	• Significant intersections are noted in logging and checked with assay results by company personnel both on site and in Perth. Diamond drilling confirms the width of the mineralised intersections. • There are no twinned holes drilled as part of these results. • All primary data is logged either digitally or on paper and later entered into an SQL database. Data is visually checked for errors before being sent to an external database manager for further validation and uploaded into an offsite database. Hard copies of original drill logs are kept in onsite office. • Visual checks of the data are completed in Datamine RM™ and Leapfrog Geo™ mining software. • No adjustments have been made to assay data unless in instances where standard tolerances are not met, and re-assay is ordered.

Criteria	JORC Code explanation	Commentary
Location of data points	• Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control.	• Diamond Drilling conducted prior to 2024 was downhole surveyed with a Champ Gyro north seeking solid state survey tool sampling every 5m, before changing over to a Devi Gyro Overshot Express tool. Continuous surveys are completed downhole when retrieving the tube at 15m, 30m, 50m, and every 50m after unless otherwise specified. An EOH continuous survey is also completed with measurements every 3m. All EOH surveys are validated by comparing the 'in' run against the 'out' run. • The RC drill holes used a REFLEX GYRO with survey measurements every 5m. • A Champ Discover magnetic multi-shot drill hole survey tool has also been utilised for comparison on some holes taking measurements every 30m. • Surface RC/DD drilling is marked out using GPS and final pickups using DGPS collar pickups • The project lies in MGA 94, zone 52. • Topographic control uses DGPS collar pickups and external survey RTK data and is considered adequate for use. • Pre Pantoro Gold survey accuracy and quality is assumed to be industry standard.
Data spacing and distribution	• Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. • Whether sample compositing has been applied.	• The underground infill and extensional drilling was conducted from a common collar location from underground and was targeted to achieve a drillhole spacing of 25-30m depending on pre-existing hole positions. • This surface drilling was nominally on 25m northing lines and spacing was between 10-30m across section lines depending on pre-existing hole positions. • No compositing is applied to diamond drilling or RC sampling. • Core samples are sampled to geology of between 0.15 and 1.2m intervals. • All RC samples are collected at 1m intervals.
Orientation of data in relation to geological structure	• Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. • If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	• Drilling is generally perpendicular to the orebody where possible, other than the limitations introduced by the need to drill fans and access limitations imposed by existing workings. All intervals are reviewed relative to the understanding of the geology and true widths calculated and reported in the tables attached in the body of the report. • Key mineralised structures vary in orientation, but are generally moderately dipping at 65° towards 075° TN. • No bias of sampling is believed to exist through the drilling orientation. • A number of the reported holes are drilled at an oblique angle to the strike of the ore and true widths have been calculated and reported in the table accompanying this report.

Criteria	JORC Code explanation	Commentary
Sample security	• The measures taken to ensure sample security.	• The chain of custody is managed by Pantoro Gold employees and contractors. Samples are stored on site in a secured area and delivered in sealed bags to both the onsite and external laboratories. • Samples are tracked during shipping. • Pre Pantoro Gold sample security is assumed to be consistent and adequate.
Audits or reviews	• The results of any audits or reviews of sampling techniques and data.	• No audit or reviews of current sampling techniques have been undertaken however the data is managed by an offsite data scientist who ensures all internal checks/protocols are in place. • Drillhole data was previously managed in Datashed™. Following an internal review, the company transitioned data management to the Plexer™ platform in early 2025. Standard validation and verification procedures were completed as part of the migration process.

Section 2: Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. • The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	• The tenement where the drilling has been completed is 100% held by Pantoro Gold. This is: M63/36. • The tenement is in good standing, and no known impediments exist.
Exploration done by other parties	• Acknowledgment and appraisal of exploration by other parties.	• Gold was discovered in the area 1894 and mining undertaken by small Syndicates. • In 1935 Western Mining established a presence in the region and operated the Mainfield and Northfield areas under the subsidiary company Central Norseman Gold Corporation Ltd. The Norseman asset was held within a company structure whereby both the listed CNGC held 49.52% and WMC held a controlling interest of 50.48%. They operated continuously until the sale to Croesus in October 2001 who then operated until 2006. During the period of Croesus management, the focus was on mining from the Harlequin and Bullen Declines accessing the St Pats, Bullen and Mararoa reefs. Open Pits were HV1, Daisy, Gladstone, and Golden Dragon with the focus predominantly on the high-grade underground mines. • From 2006-2016 the mine was operated by various companies with exploration being far more limited than that seen in previous years. • The Scotia deposit was drilled by CNGC who mined the deposit by both open pit and underground methods between 1987 and 1996.

Criteria	JORC Code explanation	Commentary
Geology	• Deposit type, geological setting and style of mineralisation.	• The Norseman gold deposits are located within the southern portion of the Eastern Goldfields Province of Western Australia in the Norseman-Wiluna greenstone belt in the Norseman district. Deposits are predominantly associated with near north striking easterly dipping quartz vein within metamorphosed Archean mafic rocks of the Woolyeenyer Formation located above the Agnes Venture slates which occur at the base. • The principal units of the Norseman district are greenstones which are west dipping and interpreted to be west facing. The sequence consists of the Penneshaw Formation comprising basalts and felsic volcanics on the eastern margin bounded by the Buldania granite batholith, the Noganyer Iron Formation, the Woolyeenyer formation comprising pillow basalts intruded by gabbros and the Mount Kirk Formation a mixed assemblage. • The mineralisation is hosted in quartz reefs in steeper shears and flatter linking sections, more recently significant production has been sourced from NNW striking reefs known as cross structures (Bullen). Whilst several vein types are categorised, the gold mineralisation is predominantly located in the main north trending reefs which in the Mainfield area strike for over a kilometre in length. The quartz/sulphide veins range from 0.5 metres up to 2 metres thick; these veins are zoned with higher grades occurring in the laminated veins on the margins and central bucky quartz which is white in colour. Bonanza grades are associated with native gold and tellurides with other accessory sulphide minerals being galena, sphalerite, chalcopyrite, pyrite and arsenopyrite. • The long-running operations at Norseman have provided a good understanding of the controls of mineralisation as well as the structural setting of the deposits. The overall geology of the Norseman area is well understood with 3D Fractal Graphic mapping and detailed studies, adding to a good geological understanding to the area. The geometry of the main lodes at Norseman are well known and plunge of shoots predictable in areas, however large areas remain untested by drilling with the potential for new spurs and cross links high. Whilst the general geology of lodes is used to constrain all wireframes, predicting continuity of grade has proven to be difficult at the higher grades when mining and in some instances (containing about 7% of the ounces) subjective parameters have been applied. • The mineralisation at Scotia is hosted by a shear zone that transects the Woolyeenyer Formation, with various types of intruding dykes. The rocks differ from that at Norseman, in that the stratigraphy were formed at higher metamorphic grades, and at a higher temperature for alteration minerals. • Gold mineralisation is hosted by a D3 ductile shear zone striking north north-west and north, dipping east. Within the mine workings this follows a north striking, east dipping gabbroic dyke.

Criteria	JORC Code explanation	Commentary
Geology (continued)		• The gold mineralisation is characterised by diversity of styles, geometry, and gold tenor. Primary gold is hosted within laminated to massive quartz-amphibole-chlorite-carbonate-pyrrhotite-chalcopyrite bearing veins that are strongly discontinuous, boudinaged (i.e. pinch & swell) and display parasitic folds. The veins are hosted within biotite-pyrrhotite-pyrite altered shear zones and form a stacked shear bounded sheeted vein system. • The dominant gold trend is represented by NNW-SSE-striking shear zones and quartz reefs which are generally moderately dipping at 60° towards 075° TN. Basalt and basalt-dolerite contacts are the preferred host-rocks to the lode shear zones. Biotite-amphibole-sulphide (pyrrhotite-chalcopyrite-arsenopyrite) wallrock alteration of the shear zones is critical for gold mineralisation.
Drill hole Information	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: » easting and northing of the drill hole collar » elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar » dip and azimuth of the hole » down hole length and interception depth » hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• A table of drill hole data pertaining to this release is attached. • All holes with results available since the last public announcement are reported.
Data aggregation methods	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Reported drill results are uncut. • All relevant intervals to the reported mineralised intercept are length weighted to determine the average grade for the reported intercept. • All significant intersections are reported with a lower cut off of 1 g/t Au including a maximum of 2m of internal dilution. Individual intervals below this cut off are reported where they are considered to be required in the context of the presentation of results. • No metal equivalents are reported.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• Drilling from the underground is drilled from static locations which means there are variable dips and azimuths due to access limitations. Surface RC/DD drilling is generally conducted perpendicular to the orebody where drill access allows it. • True widths are calculated and reported for drill intersections which intersect the lodes obliquely. • Downhole lengths are reported and true widths are calculated in both 3D using trigonometry and cartographic planes (section and plan view) using a formula in Excel.
Diagrams	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Appropriate diagrams are included in the report.
Balanced reporting	• Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	• All drill results available since the last public announcement are included in the tables. • Diagrams show the location and tenor of both high and low grade samples. • For reporting of historic drill hole intervals, holes relevant to the area of interest have been annotated where appropriate.
Other substantive exploration data	• Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	• No other meaningful data to report.
Further work	• The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). • Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	• These drill results are part of ongoing grade control and extensional drilling to infill and extend the known Scotia Mineral Resource.

Appendix 3 – Mineral Resource & Ore Reserve

Scotia Undeground Mine Mineral Resource

	Measured			Indicated			Inferred			Total		
	kT	Grade	kOz	kT	Grade	kOz	kT	Grade	kOz	kT	Grade	kOz
Scotia Underground Mine	161	8.0	42	1,021	5.8	189	743	4.1	99	1,900	5.3	329

Norseman Gold Project Mineral Resource

	Measured			Indicated			Inferred			Total		
	kT	Grade	kOz	kT	Grade	kOz	kT	Grade	kOz	kT	Grade	kOz
Total Underground	641	12.8	263	2,544	12.0	981	2,978	10.1	969	6,162	11.2	2,214
Total Surface South	140	2.3	10	12,128	1.6	628	12,765	2.6	1,087	25,043	2.1	1,727
Total Surface North	4,165	0.7	100	4,412	2.0	289	3,412	2.5	271	11,990	1.7	660
Total	**4,946**	**2.4**	**374**	**19,084**	**3.1**	**1,898**	**19,155**	**3.8**	**2,327**	**43,194**	**3.3**	**4,601**

Norseman Gold Project Ore Reserve

	Proven			Probable			Total		
	kT	Grade	kOz	kT	Grade	kOz	kT	Grade	kOz
Underground	400	6.1	79	1,846	4.8	282	2,247	5.0	360
Open Pit - Northern Mining Centres	0	0.0	0	2,140	2.2	153	2,140	2.2	153
Open Pit - Southern Mining Centres	0	0.0	0	4,076	1.8	240	4,076	1.8	240
Stockpiles	4,165	0.8	100	148	1.2	6	4,313	0.8	106
Total	**4,565**	**1.2**	**179**	**8,211**	**2.6**	**680**	**12,777**	**2.1**	**859**

Notes

- All Open Pits (0.5 g/t cut-off applied) excluding Gladstone-Everlasting (0.7 g/t cut-off applied, OK and Scotia Underground Mines (2.0 g/t cut-off applied).
- Measured and Indicated Mineral Resources are inclusive of those Mineral Resources modified to produce the Ore Reserves.
- Norseman Underground (2.5 g/t cut-off grade applied to stoping, 1.0 g/t cut-off grade applied to development necessarily mined to access stope block). Open Pits (0.6 g/t cut-off grade applied).
- Mineral Resource and Ore Reserve statements have been rounded for reporting.
- Rounding may result in apparent summation differences between tonnes, grade and contained metal content.

Appendix 4 – Compliance Statements

Exploration Targets, Exploration Results

The information in this report that relates to Exploration Targets and Exploration Results is based on information compiled by Mr Scott Huffadine, a Competent Person who is a Member of the Australian Institute of Geoscientists. Mr Huffadine is a full time employee of the company. Mr Huffadine is eligible to participate in short and long term incentive plans of and holds shares and options in the Company. Mr Huffadine has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Huffadine consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

Previous Drill Results

The information is extracted from the reports entitled "Scotia drilling confirms high grade gold extensions" created on 16 December 2024 and "Scotia Underground Depth Extensions Confirmed" created on 4 December 2025 and are available to view on Pantoro's website (www.pantoro.com.au) and the ASX (www.asx.com.au). The company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcements.

Mineral Resources and Ore Reserves

This announcement contains estimates of Pantoro Gold's Ore Reserves and Mineral Resources, as well as estimates of the Norseman Gold Project's Ore Reserves and Mineral Resources. The information in this announcement that relates to the Ore Reserves and Mineral Resources of Pantoro Gold has been extracted from a report entitled 'Annual Mineral Resource & Ore Reserve Statement' announced on 22 September 2025, and the information that relates to the Ore Reserve of the O'Briens Underground has been extracted from a report entitled 'Annual Mineral Resource and Ore Reserve Statement announced on 26 September 2022, and are available to view on the Company's website (www.pantoro.com.au) and www.asx.com (Mineral Resource & Ore Reserve Announcements).

For the purposes of ASX Listing Rule 5.23, Pantoro Gold confirms that it is not aware of any new information or data that materially affects the information included in this Mineral Resource & Ore Reserve Announcements and, in relation to the estimates of Pantoro Gold's Ore Reserves and Mineral Resources, that all material assumptions and technical parameters underpinning the estimates continue to apply and have not materially changed. Pantoro Gold confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from that announcement.

Forward Looking Statements

Certain statements in this report relate to the future, including forward looking statements relating to Pantoro's financial position and strategy. These forward looking statements involve known and unknown risks, uncertainties, assumptions and other important factors that could cause the actual results, performance or achievements of Pantoro to be materially different from future results, performance or achievements expressed or implied by such statements. Actual events or results may differ materially from the events or results expressed or implied in any forward looking statement and deviations are both normal and to be expected. Other than required by law, neither Pantoro, their officers nor any other person gives any representation, assurance or guarantee that the occurrence of the events expressed or implied in any forward looking statements will actually occur. You are cautioned not to place undue reliance on those statements.