ASX ANNOUNCEMENT

02 May 2017

STRANDLINE
resources limited

High Value Fungoni Mineral Resource Continues to Expand

HIGHLIGHTS:

- **Significant increase to Fungoni Mineral Resource Estimate –** Extension drilling of the Fungoni north-west zone (**Fungoni NW**) has successfully grown the global Fungoni Mineral Resource and confirmed the continuity of the higher grade, zircon dominated upper zone:
    - **38% increase** (up ~6Mt) in the global Mineral Resource to **21.7Mt @ 2.82%** Total Heavy Mineral (**THM**) at a 1% THM cut-off, previously 16Mt @ 3.1% THM;
    - **27% increase** (up ~130,000t) in contained Heavy Mineral (**HM**) to over **610,000t** from previous 480,000t;
    - Upper zone core of mineralisation **10.8Mt @ 4.4% THM** for 472,000t of HM at a 1.5% THM cut-off, comprising 42.4% Ilmenite, 18.3% zircon, 4.5% rutile and 1.2% leucoxene; and
    - **High degree of confidence** in the Mineral Resource with **41% Measured and 59% Indicated**, with both categories suitable for Ore Reserve estimation and detailed mine plan optimisation.
- **Preliminary Mining study promises to improve project metrics –** Mine optimisation analysis by AMC Consultants confirms efficient mining from surface, targeting the higher grade upper zone to achieve a significant improvement on the previous Fungoni engineering study in terms of a higher mining rate and increased tonnes of recovered valuable HM for the Project.
- **Exploration continues in the broader Fungoni Region** with a surface geochemical sampling programme of radiometric anomalies and known mineralised trends identifying prospective high grade mineralised zones in close proximity to the Fungoni Project - sample assaying and assemblage testwork to commence soon, followed by Aircore drilling.

Mineral sands developer, Strandline Resources (**Strandline** or **the Company**) is pleased to provide an update on its 100% owned Fungoni Heavy Mineral Sands (**HMS**) Project, located near Dar es Salaam in Tanzania.

This update to the Fungoni Mineral Resource estimate includes the recently discovered Fungoni NW extension zones adding significant HM tonnage to the ore-body.

The mining study, currently underway, will incorporate this new Resource and targets a substantial improvement to the previous Fungoni study in terms of mining rate, HM tonnage, mine life and ultimately project economics.

COMMENTARY:

Strandline's Managing Director and CEO, Luke Graham commented, *"The Company has successfully doubled the size of the Fungoni Mineral Resource estimate since the start of the year, from 11Mt to now 22Mt, and significantly increased the contained HM available for DFS level mine optimisation.*

"The Company expects strong conversion to Ore Reserve of the higher grade upper zones where the majority of valuable, high quality heavy minerals reside. The visual results from the recent soil sampling exercise in proximity to the Fungoni Project is also encouraging, showing potential to further expand Resources in the area over time.

"The Company is excited by the near term project potential of Fungoni as well as progress made on the Company's other strategic project pursuits in Tanzania in an improving Mineral Sands Market."

INTRODUCTION

Strandline continues to advance development of its zircon-rich Fungoni Mineral Sands Project, located 25km south of Dar es Salaam port infrastructure (Figure 1). The Project is predicated on a **low capital cost** and **fit-for-market** operating model to produce saleable zircon, rutile and ilmenite HMS products to generate near-term cashflow for the Company.

Results from Strandline's extensional drill programme, along strike from Fungoni towards Fungoni NW showed zones of mineralisation comparable to the main Fungoni mineralised body. These new zones of mineralisation have now been included in this global Mineral Resource update and supersede the results previously released on 16 January 2017. The infill drilling has been successful in delineating additional high grade zones with a high proportion of high unit value minerals that include zircon, rutile and leucoxene.

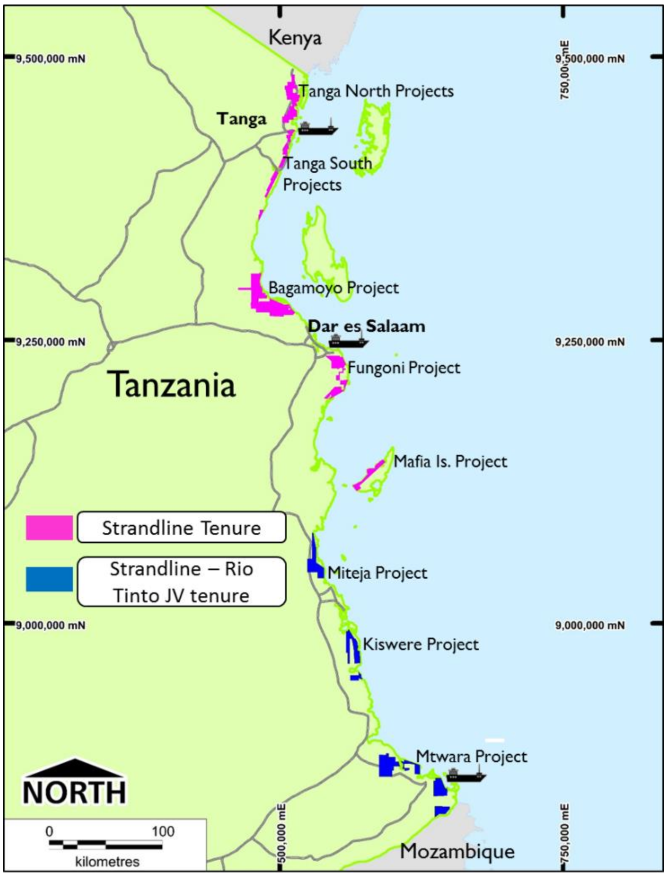


Figure 1 - Strandline holds a large tenement package strategically located along the Tanzanian Coastline

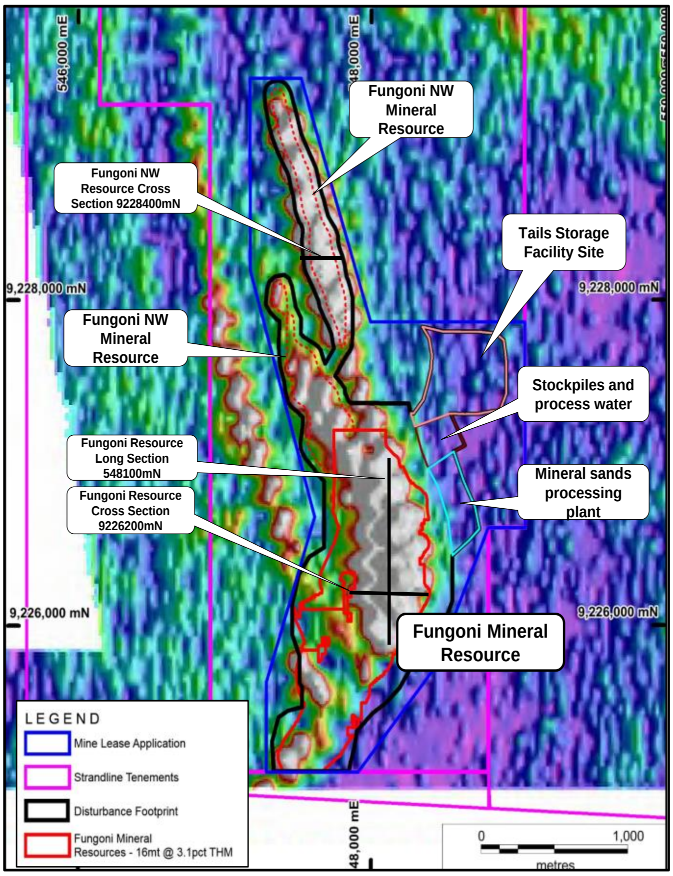


Figure 2 - Location Map of the Fungoni Mineral Resource and contiguous NW Radiometric Anomaly (titled **Fungoni NW**)

FUNGONI PROJECT JORC-2012 MINERAL RESOURCE UPDATE

The Mineral Resource estimation was conducted by Greg Jones who is a full time employee of IHC Robbins, a specialist consultant in mineral sands resources, metallurgy and processing (refer to Competent Person statement).

Table 1 below displays the Mineral Resources estimated for the Global Fungoni HMS Project. Importantly, the mineral resources are classified as Measured and Indicated and all commence at surface with nil, to extremely low, strip ratios.

Table 1 – Global Mineral Resource Statement for Fungoni at May 2017

MINERAL RESOURCE SUMMARY FOR FUNGONI PROJECT										
Summary of Mineral Resources[1]					VHM assemblage[2]					
Deposit	**Mineral Resource Category**	**Tonnage**	**In situ THM**	**THM**	**Ilmenite**	**Rutile**	**Zircon**	**Leucoxene**	**Slimes**	**Oversize**
		(Mt)	(Mt)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
FUNGONI	Measured	8.77	0.37	4.26	43.3	4.3	18.3	1.0	18.5	6.8
FUNGONI	Indicated	12.97	0.24	1.84	36.7	4.3	14.6	1.4	24.4	7.3
	Total[3]	21.74	0.61	2.82	40.7	4.3	16.9	1.2	22.0	7.0
(1) Mineral Resources reported at a cut-off grade of 1.0% THM										
(2) Valuable Mineral assemblage is reported as a percentage of in situ THM content										
(3) Appropriate rounding applied										
(4) Refer to Appendix 3 for detailed breakdown by zone of Trash and VHM										

Grade tonnage curves are presented in Figures 3 and 4.

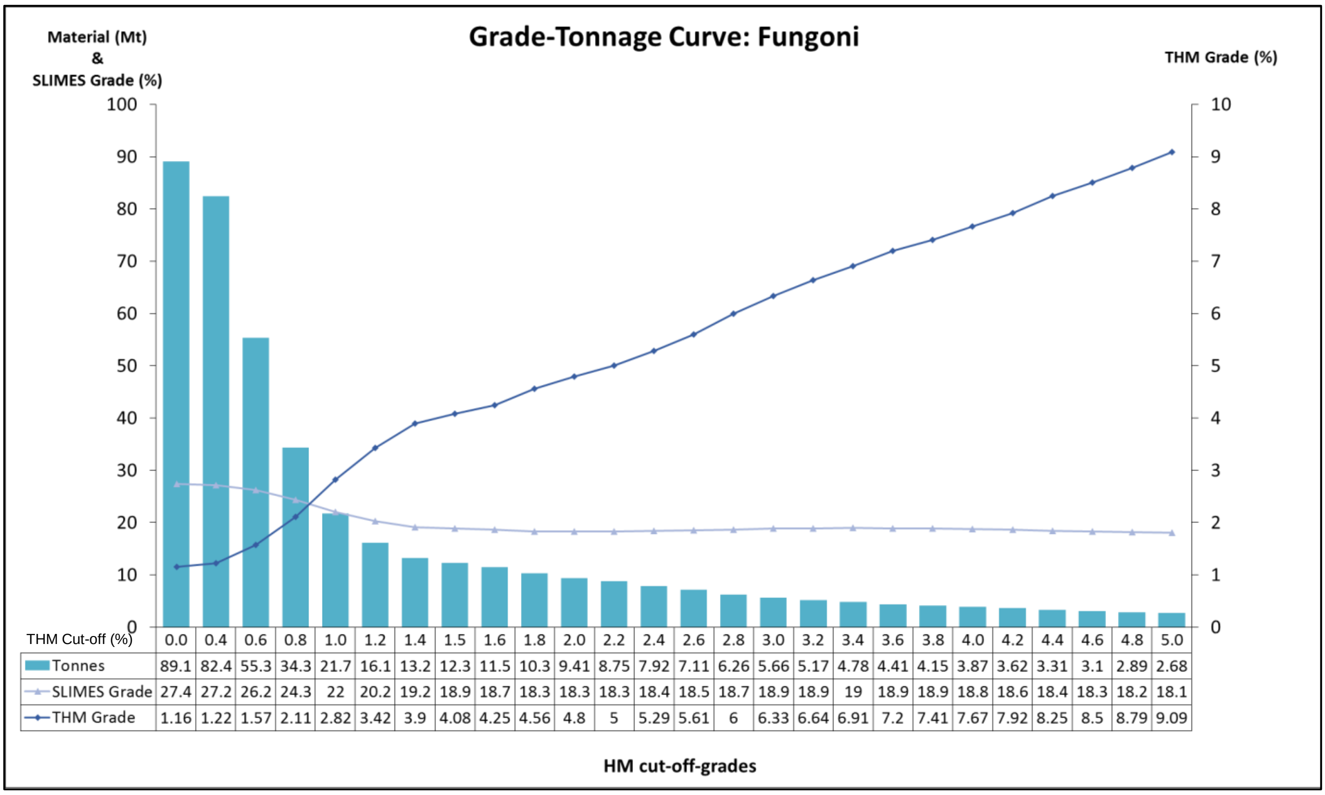
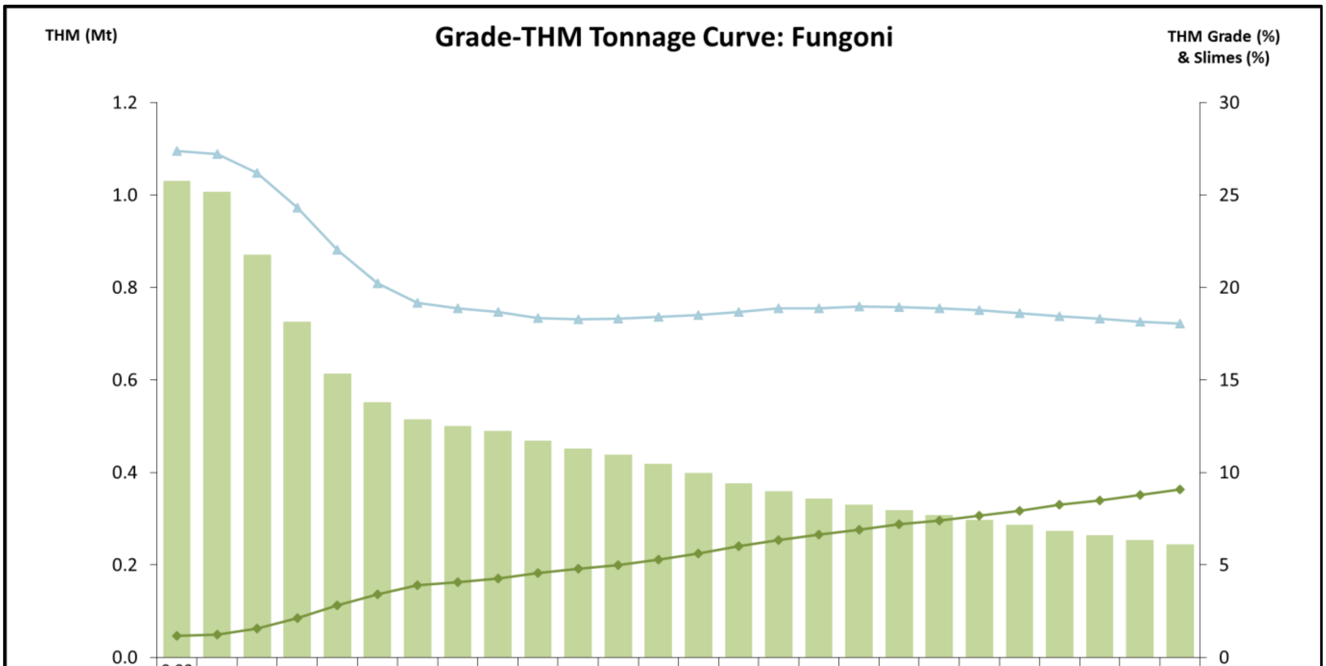


Figure 3 - Grade-tonnage curve for the Fungoni deposit (including Fungoni NW)



THM Cut-off (%)	0.00 001	0.4	0.6	0.8	1	1.2	1.4	1.5	1.6	1.8	2	2.2	2.4
THM Tonnes	1.03	1.01	0.87	0.72	0.61	0.55	0.51	0.5	0.49	0.47	0.45	0.44	0.42
THM Grade	1.16	1.22	1.57	2.11	2.82	3.42	3.9	4.08	4.25	4.56	4.8	5	5.29
SLIMES Grade	27.4	27.2	26.2	24.3	22	20.2	19.2	18.9	18.7	18.3	18.3	18.3	18.4

THM Cut-off (%)	2.6	2.8	3	3.2	3.4	3.6	3.8	4	4.2	4.4	4.6	4.8	5
THM Tonnes	0.4	0.38	0.36	0.34	0.33	0.32	0.31	0.3	0.29	0.27	0.26	0.25	0.24
THM Grade	5.61	6	6.33	6.64	6.91	7.2	7.41	7.67	7.92	8.25	8.5	8.79	9.09
SLIMES Grade	18.5	18.7	18.9	18.9	19	18.9	18.9	18.8	18.6	18.4	18.3	18.2	18.1

Figure 4 - Grade-THM curve for the Fungoni deposit (including Fungoni NW)

The Fungoni Project has a Measured and Indicated global Mineral Resource of 21.7 million tonnes @ 2.82% Total Heavy Minerals (**THM**) for a contained HM of 610,000t, and an overall valuable assemblage of 4.3% rutile, 1.2% leucoxene, 16.9% zircon and 40.7% ilmenite at a cut-off grade of 1.0% THM. Slime (defined as silt <45µm) content at this cut-off is 22%.

There has been a 38% increase (up 6Mt) in the global Mineral Resource estimate to 22Mt @ 2.8% THM from the previous equivalent Measured and Indicated Mineral Resource of 16Mt @ 3.1% THM. This has resulted in a 27% increase (up 130,000t) in the contained HM tonnes over the previous resource estimate from 480,000t to 610,000t.

Within upper Zone 2, continuous zones of elevated mineralisation of 10.8Mt @ 4.4% THM is comprised of 42.4% Ilmenite, 18.3% zircon, 4.5% rutile and 1.2% leucoxene using a 1.5% THM cut-off.

The overall Fungoni Mineral Resource is exposed at surface (Figures 5), with the mineralised body showing strong geological continuity along strike and at depth. Low strip ratios are anticipated from the mining model with a large portion of the high-grade mineral resource favourably positioned at surface. Cross sections and a long section are presented in Figures 6, 7 and 8 as referenced in Figure 2.

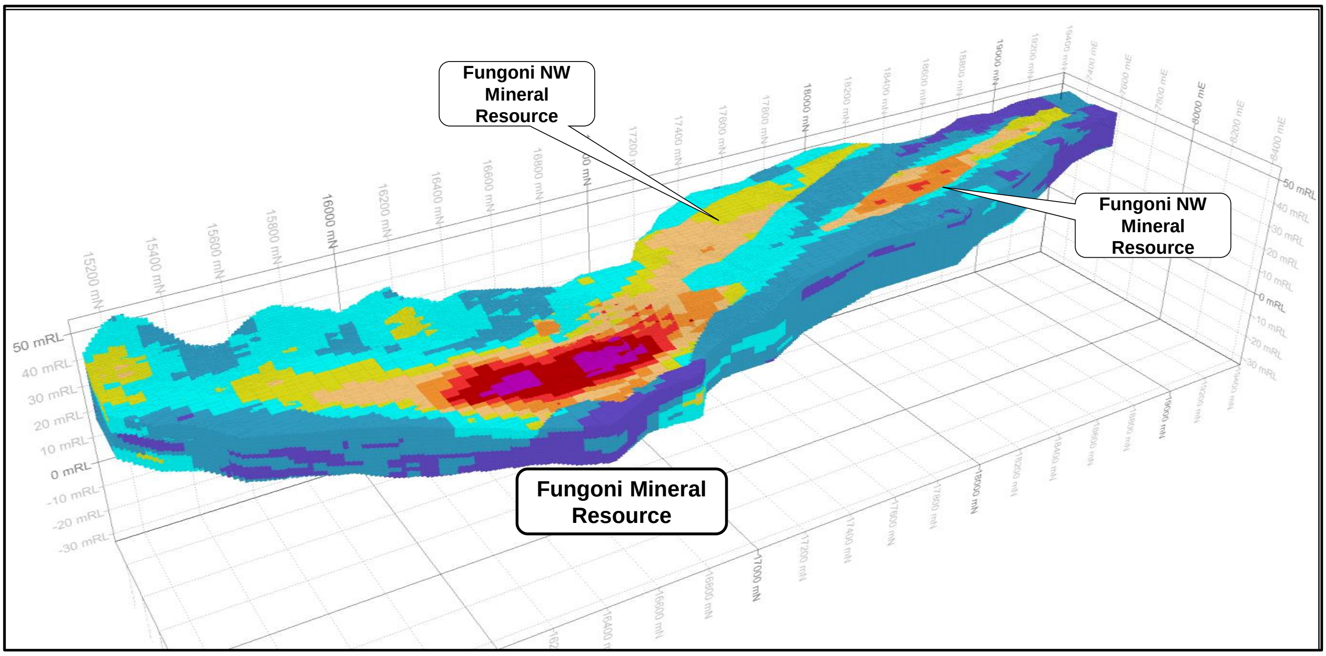


Figure 5 - Fungoni Mineral Resource block model – view looking west north west

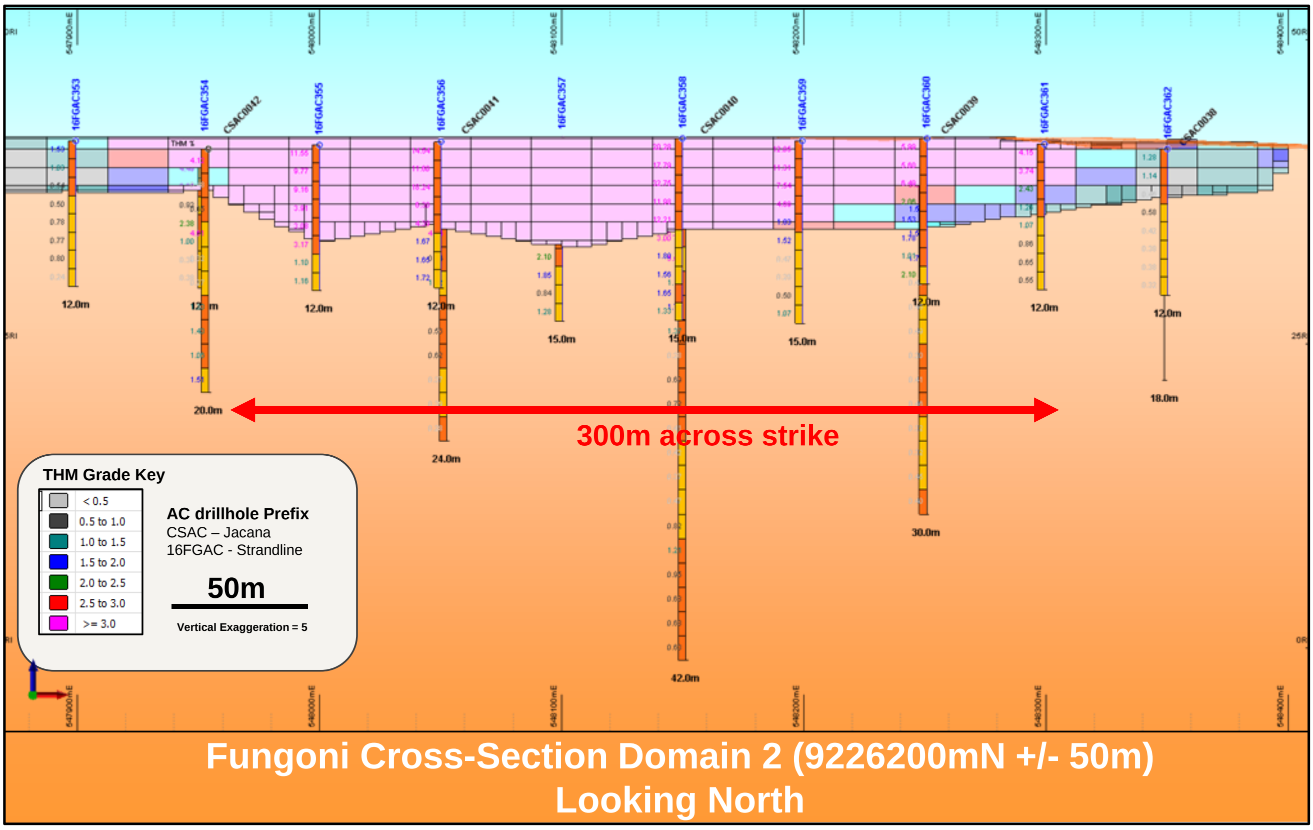


Figure 6 - Cross section through the centre of the Fungoni Mineral Resource.

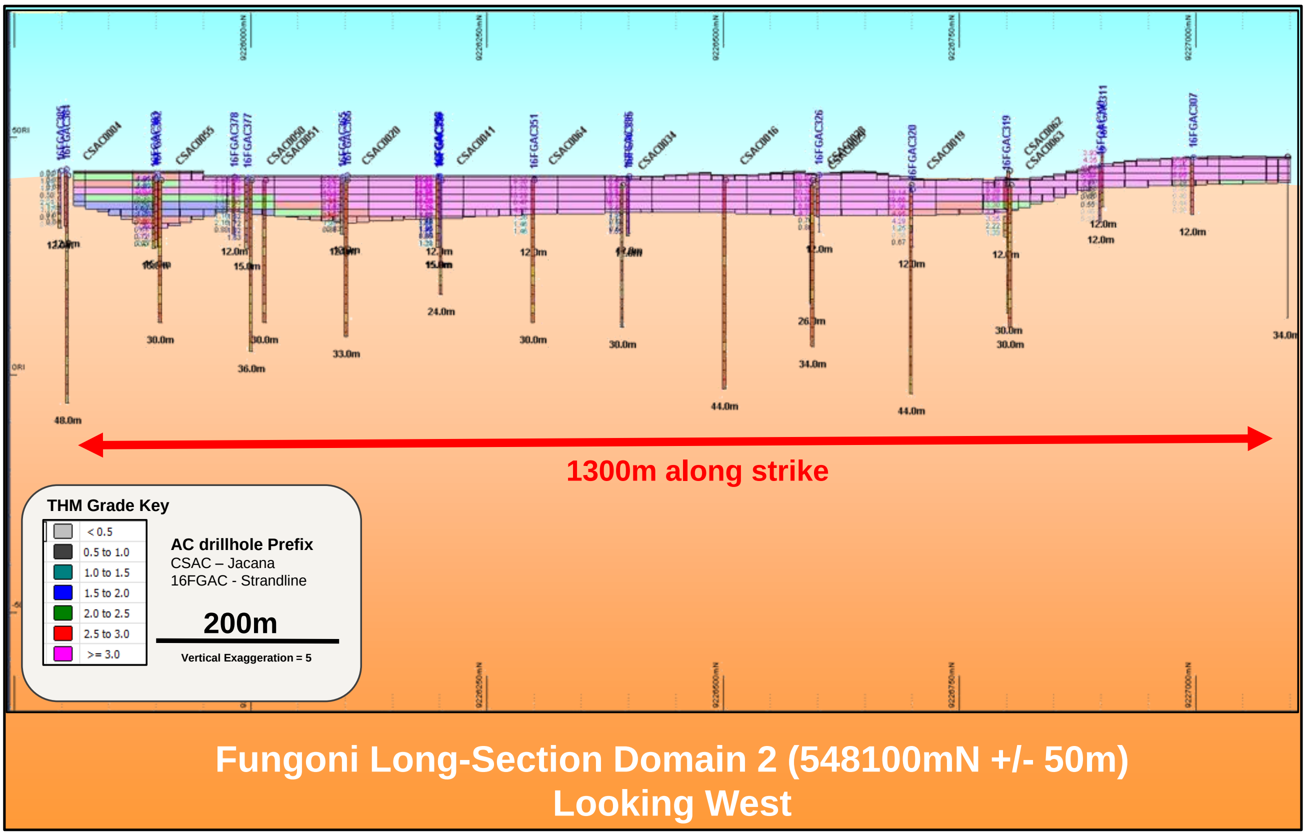


Figure 7 - Long section through the centre of the Fungoni Mineral Resource.

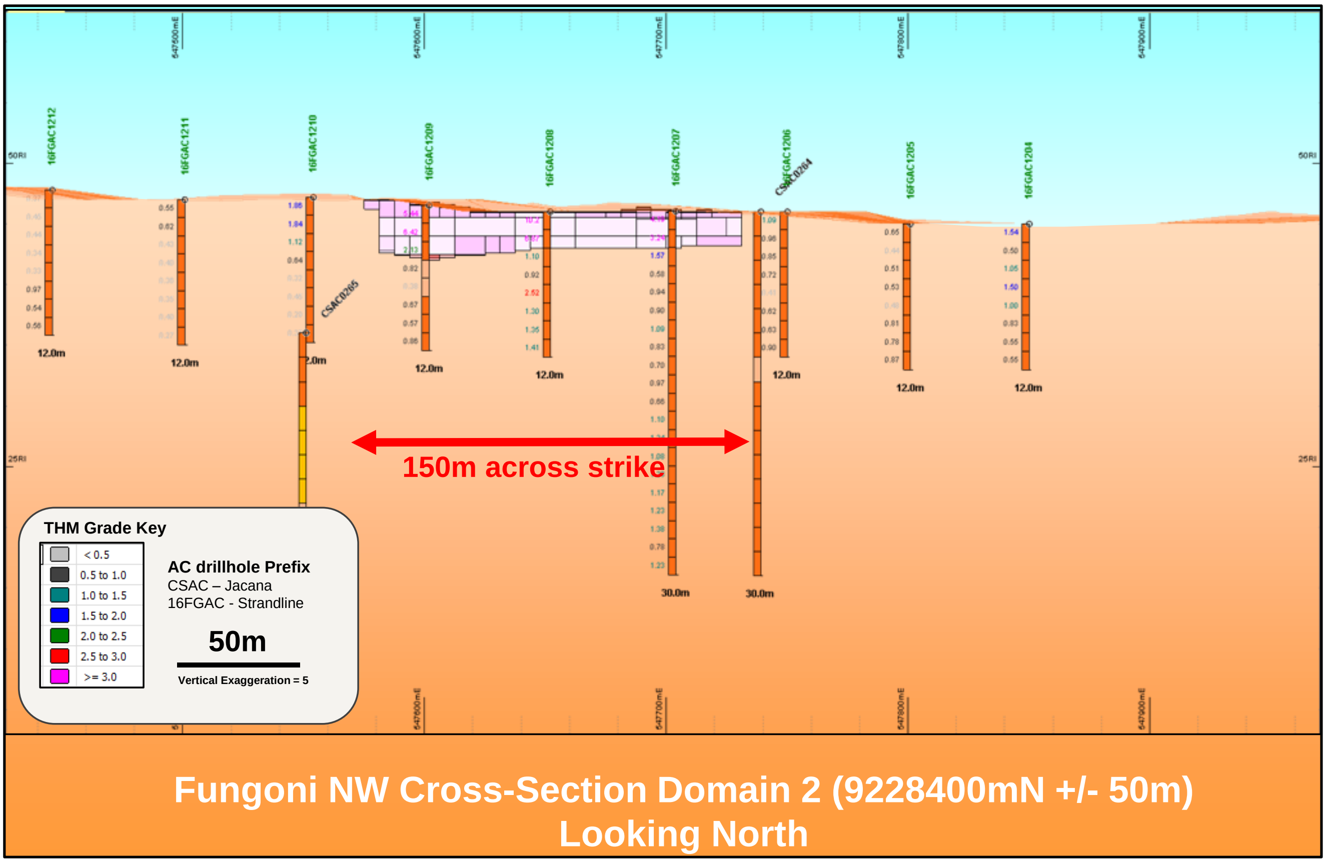


Figure 8 - Cross section through the centre of the Fungoni NW Mineral Resource.

SUMMARY OF RESOURCE ESTIMATE AND REPORTING CRITERIA

As per ASX Listing Rule 5.8 and the 2012 JORC Code reporting guidelines, a summary of the material information used to estimate the Mineral Resource is detailed below (for more detail please refer to JORC Table 1, Sections 1 to 3 included in Appendix 1).

Geology and geological interpretation

In Tanzania two main types of heavy mineral placer style deposits have potential for resources delineation:

1. Thin but high grade strandlines which may be related to marine or fluvial influences; and
2. Large but lower grade deposits related to windblown sands.

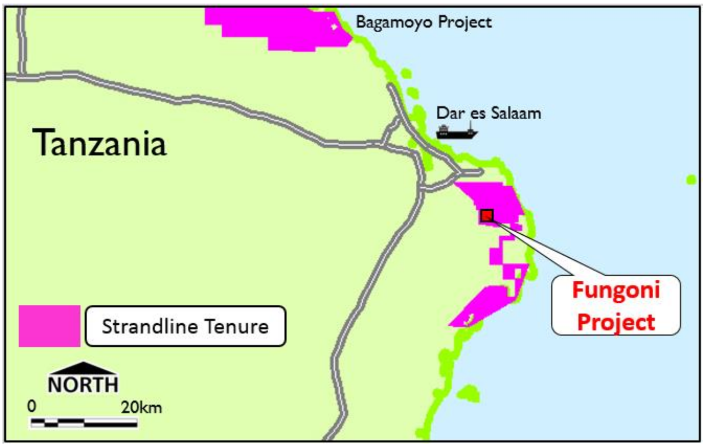


Figure 9 - Fungoni Project Location, Central Coast Tanzania

The surface geology of the tenement comprises grey to white sandy soils within and overlying a thicker mixed sedimentary sequence. The majority of the Fungoni resource is situated within an arcuate shaped depression at the base of a ten metre rise to the west. The mineralisation is shown to extend up and over this topographic rise towards the north-west where heavy mineral sand was previously identified and drilled (Fungoni NW). This new mineralisation is the subject of this Mineral Resources update.

The higher grade domains of the resource are defined by more dominant valuable minerals such as zircon, ilmenite and rutile in addition to kyanite/sillimanite. Higher grade domains 2 and 4 are also characterised by typically more sandy soils with lower slimes content. The boundary to the underlying lower grade domain 5 is marked by a noticeable increase in the slimes content and decrease in valuable mineral content with the introduction of garnet to the trash component of the THM. Within both domains, there are a series of interbedded course sandy units which maybe fining upwards to silt and clay potentially within an alluvial influenced setting. Additional sedimentological studies will be required to further develop the geological model.

Drilling techniques and hole spacing

The aircore drilling technique was used to drill the Fungoni and Fungoni NW areas. Aircore is considered a standard industry technique for evaluating HMS mineralisation and is a form of reverse circulation drilling where the sample is collected at the drill bit face and returned inside the inner tube. The drill bit is 76 mm in diameter (NQ) and the rods are 3m long. All the holes were drilled vertically.

The previous resource drilling density completed at Fungoni was on a 100 m x 100 m grid. This has been reduced to a 100 m x 50 m grid with twinning of 31 previous drill holes to assist in the verification of the older Jacana data. At Fungoni NW the resource was drilled on a 200 x 50m grid pattern. A high degree of confidence in the geological model and grade continuity between drill holes has been established at Fungoni and Fungoni NW which supports the mineral resource classification assigned to each area.

For geological interpretation and resource modelling a local grid was set up along the long axis of the deposits so that the majority of drill lines were east-west and model cells were aligned north-south along that long axis. This allows for a simplification of the geological interpretation and subsequent model preparation, interpolation and analysis. The orientation of the grid was such that only a translation of X and Y co-ordinates was required and no rotation was used.

Sampling and sub-sampling techniques

Aircore drilling was used to obtain samples at 1.5 m intervals, which generated about 8kg of drill spoil that was progressively split down to 1000 g using a three tier riffle splitter. The smaller split samples were labelled and bagged for export to the primary laboratory for processing. Any wet or damp samples were allowed to dry prior to the splitting stage. The sampling method and sample size dispatched for processing is considered appropriate and reliable based on accepted industry practices and experience.

A sample ledger is kept at the drill rig for recording sample intervals and sample mass, and photographs are taken of samples for each hole to cross-reference with logging.

There were two phases of drilling undertaken on the Fungoni Project, by Jacana/Syrah in 2012 and by Strandline in 2016. Only one phase of drilling was completed at Fungoni NW although Jacana/Syrah did drill a number of holes across the NW zone but these were not assayed for THM. A breakdown of the drilling metres, samples taken and assays submitted and then subsequently used in the Mineral Resource estimate is shown in Table 2 with >1% THM intersects tabulated in Appendix 2.

Table 2 - List of drill holes, samples and assays by drill programme

Deposit	Drilling Co.	Drill Series	Method	Date	Holes	Metres	Samples	Assays	Assayed
Fungoni	Wallis	CSA	Air Core	2012	117	3,698	1,717	1,089	63%
Fungoni	Wallis	CSA	Air Core	2016				340	20%
Fungoni	Wallis	16FGA	Air Core	2016	277	3,579	2,386	2,386	100%
Total					**394**	**7,277**	**4,103**	**3,815**	**93%**

Some select samples from the 2012 drilling programme were located and re-submitted for assay by Strandline.

Sample analysis method - THM

The 1000 g samples representing 1.5 m drill intervals were analysed by Western Geolabs in Perth, Western Australia, which is considered the primary laboratory for this resource estimate. The 1000 g samples were initially sieved to remove the +3 mm fraction and the weight recorded and then split to 250 g which was soaked overnight and screened for removal and determination of Slimes (-45 µm) and Oversize (+1 mm). The residual 45 µm to 1 mm fraction was then micro-riffle split down to approximately 100 g which was analysed for THM using tetrabromoethane (TBE) as the liquid heavy media. The density range of TBE is 2.92 and 2.96 g/cm3. This is an industry standard process used to determine heavy mineral contents.

Sample analysis method - mineral assemblage

Mineral assemblage composites are used to prepare weighted average assays of mineralogy and mineral species chemistry for designated zones or domains within an ore body. For the Fungoni Project two assay methods were used to determine THM mineralogy although the rationale for selection of drill samples to make up individual composites was the same. The identification and selection of individual samples was conducted as follows:

- Detailed sachet scanning of heavy mineral sinks from the drill assay process was carried out to determine regions of gross mineralogy as well as an overall consideration of valuable heavy mineral (VHM) content. Other considerations undertaken during this sachet logging were the presence of iron oxide coatings on THM, and any gross composition of trash HM.
- Sachet logging then formed the input to the geological/mineralogical/THM grade interpretation which was then used to drive domain control for modelling, as well as providing the guidance for the allocation of mineral assemblage composites.
- Three individual domains were identified for the purpose of guiding the allocation of composites; the upper zone (ZONE=2), the oxide zone (ZONE=4) and the lower zone (ZONE=5) (refer to Figure 8). These domains were further subdivided into north-south sample regions, with each mineral assemblage

composite collected from two drill lines approximately 100 m apart (refer Figure 10) - with the exception of the southernmost three lines that were composited together.

- For the north-west extension of Fungoni where drilling was spaced at 200 m spaced drill lines and the morphology of strands was shallower and narrower than the main deposit, the selection of composites was made over three drill lines. In the case of the lower domain (ZONE=5) the entire domain north of 17200 mN was composited together. This approach was taken for the north-west extension due to the smaller weight of material available to prepare composites for the selected mineralogy determination method.
- A total of 22 mineral assemblage composites were used to characterise the mineralogy and chemistry for the main Fungoni project and a further five composites were used to characterise the north-west extension.
- Individual drill hole samples were selected based on whether they fell within a particular domain, and were then proportioned against contained THM grade in order to specify the weight of THM that each sample would contribute to the entire composite.
- Once all of the ratio calculations were completed, the spreadsheet with sample identification and mineral assemblage composite number was submitted to Geoff Lane at Process Mineralogical Consulting Ltd (PMC) in Canada for sample collation and processing for the main Fungoni deposit, and for the north-west extension, the samples were sent to Allied Mineral Laboratory (AML) in Perth.
- Preparing the mineral assemblage composites in this manner allows for composite results to be applied to the resource block model and for those results to then be reported and weighted on THM in the final Mineral Resource estimate.
- Details of mineral assemblage composite IDs with associated results are presented in Appendix 3.

The mineral assemblage composites from the main part of the deposit were assayed using an SEM (Scanning Electron Microscope) and then an EDX (Energy Dispersive X-Ray analyser). For the purpose of this release the methodology description is shortened to SEM-EDX. The methodology is similar in some ways to Mineral Liberation Analyser (MLA) and QEMSCAN (Quantitative Evaluation of Minerals by Scanning Electron Microscopy), however the key differential is interpretation by the mineralogist to assign mineral species based on a typical scan of between 1000 and 3000 individual grains. This semi quantitative analysis, with mineralogical identification and assignment allows for a significant improvement in identifying key valuable and trash heavy mineral species along with their respective key oxide chemical constituents.

All of the VHM and trash mineral species were identified using the SEM-EDX method, with zircon calculated from whole rock XRF, which represents a more comprehensive analysis for that mineral species.

The mineral assemblage composites from the north-west extension were assayed by magnetic separation into three fractions, magnetic, para-magnetic and non-magnetic. These fractions were then assayed by XRF (X-Ray Fluorescence) to determine oxide amounts. The ratio and relationship of specific oxides to mineral species and their deportment based on magnetic properties can be used to back calculate overall mineral mass distribution. The results of this method are in alignment with the SEM-EDX results, without the specific mineral breakdown for magnetic and non-magnetic trash mineral species.

In order to report the two data set methodologies, some aggregation of the SEM-EDX mineralogy was required to align with the magnetic separation mineral assemblage. The combined data sets are shown in Appendix 3.

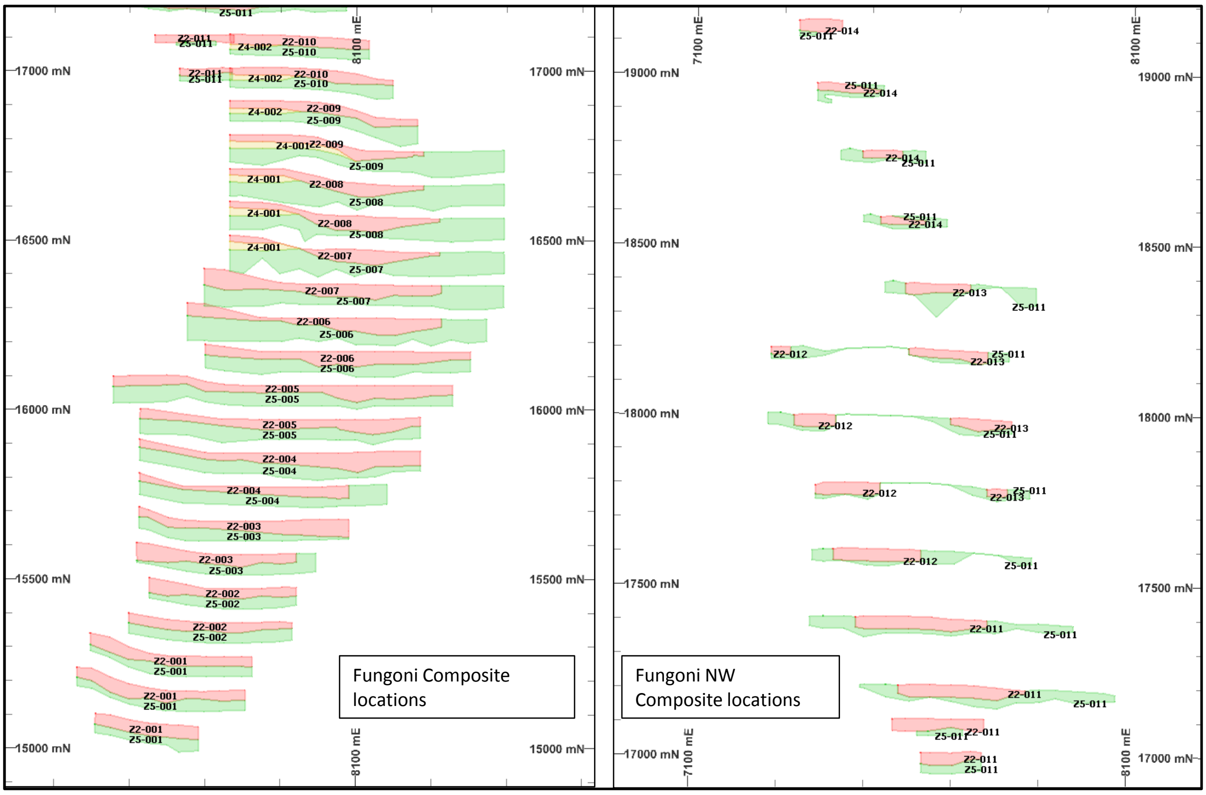


Figure 10 - Oblique Views Showing Spatial Distribution of Fungoni's and Fungoni NW Mineral Assemblage Composites. Pink upper zone, green lower zone with composite sample code assigned to each zone

Estimation Methodology

Geological interpretation, wireframing, 3D block modelling and grade interpolation was carried out using CAE Mining / Datamine Studio mining software. Construction of the geological grade model was based on a combination of coding model cells and drill holes below open wireframe surfaces, including topography and basement and inside closed wireframes defined by mineralised domains. Modelling convention has the largest parent cell size possible used which is generally based on half the distance between holes of the dominant drill hole spacing in the X and Y dimensions. Cell dimensions are generally used so as to avoid overly small cells that imply a level of refinement in the model that is not justified by the drill hole spacing. The dominant drill grid spacing for the Fungoni deposit was 100 m along strike × 50 m across strike × 1.5 m down hole for Strandline drilling. The selection of parent cell dimensions in XYZ of 25 x 50 x 1.5 m in order to have a floating cell between drill holes and drill lines.

A model was generated for the deposit and interpolated using inverse distance weighting and the preliminary estimates were compared with drill hole grades. Variography was carried out prior to interpolation as part of developing search ellipse directions and sizes. Resulting variograms were used to test the drill spacing (and continuity of HM grade) and these supported the final selected JORC Mineral Resource category.

This cell size and parameters chosen resulted in an acceptable interpolation process and this was confirmed by a comparison of the drill hole and block model grades. The search ellipse used for the grade interpolation was guided by the dynamic ellipsoid routine employed by Datamine. This allows for variations in mineralisation strike, dip and plunge to be accounted for during the grade interpolation. The mineral assemblage composite identifiers were interpolated into the block model utilising a nearest neighbour method.

A bulk density (BD) of 1.8 g/cm^3 was applied to the model using a fixed BD value based on previous work carried out on the deposit. This is considered a conservative approach and the value is well within the average range of bulk densities previously observed by the Competent Person in previous mineral sands resource estimation studies and based on operational experience.

Cut-off grades

A cut-off-grade of 1% THM was selected for the Fungoni deposit based on grade tonnage curves and the high percentage of valuable heavy mineral (VHM) most notably the elevated zircon content.

Classification criteria

The Fungoni Mineral Resource estimate has been assigned a JORC classification of Measured and Indicated Mineral Resource which is supported by the following criteria:

- drill hole spacing;
- continuity of grade and geology;
- support of variography for key primary assay grades; and
- distribution and weighting of mineral assemblage composites.

The density/number of samples and distribution of mineral assemblage composites is to an adequate level of density for the JORC classification.

The distribution of the mineral assemblage composites throughout the deposit has enabled a clear picture to be gained of the VHM grade and distribution for Fungoni and provides a solid basis for further mine optimisation and mine planning studies.

Mining and metallurgical methods and parameters

The Company has undertaken heavy mineral composite analyses of the Fungoni mineral resources which has provided detailed data for the VHM assemblage from the total heavy mineral. This information compares favourably with the closest operational mineral sands mine – Kwale, located in Kenya – owned by ASX listed company Base Resources.

A large (3t) metallurgical sample at a Life of Mine grade profile has been collected and submitted for mineral processing to enable process flowsheet design for input into the feasibility study. An update to the Market on the 30th March 2017 provided the following:

- Bulk metallurgical testwork confirms simple and practical process flowsheet for the wet concentrator and mineral separation plants, incorporating embedded design flexibility and robustness to tailor the final product suite to maximise product value, marketability and project returns;
- Preliminary flowsheets incorporate proven mineral process beneficiation and separation technology achieving excellent process performance metrics, including high recoveries for preferred products; and
- High quality final product suite to be produced suitable for the global HMS markets, including ilmenite quality favourable for the production of TiO2 pigment via the Chloride Process and high purity zircon containing very low contaminants potentially suitable for the ceramic's industry.

The Company is awaiting final reporting of the testwork and mass balance calculations which will be released once they are available.

A total of two 2.5t samples have also been collected and submitted for grade variability testwork. They comprise a lower grade sample averaging approximately 3% THM and higher grade samples with a grade of approximately 16% THM. These will be subjected to the preliminary flow sheet design and will assist in finalising processing design parameters.

For further enquiries, please contact:
Luke Graham
Managing Director
Strandline Resources Limited
T: +61 8 9226 3130
E: enquiries@strandline.com.au
Website: www.strandline.com.au

For media and broker enquiries:
Andrew Rowell
Cannings Purple
T: +61 8 6314 6314
E: arowell@canningspurple.com.au

ABOUT STRANDLINE RESOURCES

Strandline Resources Limited (**ASX: STA**) is a Tanzanian-focused mineral sands developer positioned within the world's major zircon and titanium producing corridor in South East Africa. Strandline has a dominant mineral sands position with a series of 100% owned projects spread along 350km of the Tanzanian coastline.

Strandline's strategy is to develop and operate quality, low cost, expandable mining assets with market differentiation. Leveraging off the exploration success of 2016, the Company's focus is to continue its aggressive exploration and development strategy to progress economically attractive projects based on high unit value titanium and zircon products.

Competent Person's Statements

The information in this report that relates to Exploration Results is based on, and fairly represents, information and supporting documentation prepared by Dr Mark Alvin, Exploration Manager and a full time employee of Strandline and Mr Brendan Cummins, Chief Geologist and a part time employee of Strandline. Dr Alvin is a Member of The Australasian Institute of Mining and Metallurgy and Mr Cummins is a member of the Australian Institute of Geoscientists and they both have sufficient experience which is relevant to the style of mineralisation and type of deposits under consideration and to the activity which has been undertaken to qualify as Competent Persons as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Dr Alvin and Mr Cummins consent to the inclusion in this release of the matters based on the information in the form and context in which they appear.

The information in this report that relates to Mineral Resources is based on, and fairly represents, information and supporting documentation prepared by Mr Greg Jones, and employee of IHC-Robbins and Consultant to Strandline and Mr Brendan Cummins (Chief Geologist and part-time employee of Strandline). Mr Jones is a member of the Australian Institute of Mining and Metallurgy and Mr Cummins is a member of the Australian Institute of Geoscientists and both have sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to the activities undertaken to qualify as Competent Persons as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Specifically, Mr Cummins is the Competent Person for the drill database, geological model interpretation and completed the site inspection. Mr Jones is the Competent Person for the mineral resource estimation. Mr Jones and Mr Cummins consent to the inclusion in this report of the matters based on their information in the form and context in which they appear.

Forward Looking Statements

This report contains certain forward looking statements. Forward looking statements are only predictions and are subject to risks, uncertainties and assumptions which are outside of the control of Strandline. These risks, uncertainties and assumptions include commodity prices, currency fluctuations, economic and financial market conditions, environmental risks and legislative, fiscal or regulatory developments, political risks, project delay, approvals and cost estimates. Actual values, results or events may be materially different to those contained in this announcement. Given these uncertainties, readers are cautioned not to place reliance on forward looking statements. Any forward looking statements in this announcement reflect the views of Strandline only at the date of this announcement. Subject to any continuing obligations under applicable laws and ASX Listing Rules, Strandline does not undertake any obligation to update or revise any information or any of the forward looking statements in this announcement to reflect changes in events, conditions or circumstances on which any forward looking statements is based.

Appendix 1

JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	*Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* *Aspects of the determination of mineralisation that are Material to the Public Report.* *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	Aircore drilling was used to obtain samples at 1.5m intervals for the 2016 Strandline Drilling and 2m intervals for 2012 Jacana/Syrah drilling. The following information covers the Strandline sampling process: • Each 1.5m sample was homogenized within the bag by manually rotating the sample bag • A sample of sand, approx. 20gm, is scooped from the sample bag for visual THM% estimation and logging. The same sample mass is used for every pan sample for visual THM% estimation • The standard sized sample is to ensure calibration is maintained for consistency in visual estimation • A sample ledger is kept at the drill rig for recording sample intervals and sample mass, and photographs are taken of samples bags for each hole to cross-reference with logging • The large 1.5m Aircore drill samples have an average of about 8kg and were split down to approximately 1000gm by riffle splitter for export to the primary processing laboratory • The laboratory sample was dried, screened to +3mm, de-slimed (removal of -45µm fraction) and then had oversize (+1mm fraction) removed. Approximately 100gm of sample was then split to use for heavy liquid separation using TBE to determine total heavy mineral content The following information covers the Jacana/Syrah sampling process: • 2m samples were collected • samples collected were taken to the external laboratory in South Africa (Stewart Group) • a 600 g sample was obtained from a roughly 2 to 2.5 kg sample using a riffle splitter and tested for total heavy mineral content • a single composite sample were tested for VHM using grain counting and XRF at 2 laboratories

Criteria	JORC Code explanation	Commentary
Drilling techniques	*Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	Aircore drilling with inner tubes for sample return was used Aircore is considered a standard industry technique for HMS mineralization. Aircore drilling is a form of reverse circulation drilling where the sample is collected at the face and returned inside the inner tube Aircore drill rods used were 3m long NQ diameter (76mm) drill bits and rods were used All drill holes were vertical
Drill sample recovery	*Method of recording and assessing core and chip sample recoveries and results assessed.* *Measures taken to maximise sample recovery and ensure representative nature of the samples.* *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Drill sample recovery is monitored by measuring and recording the total mass of each 1.5m sample at the drill rig with a standard spring balance. . For Jacana drilling, sample recovery was visually checked While initially collaring the hole, limited sample recovery can occur in the initial 0.0m to 1.5m sample interval owing to sample and air loss into the surrounding loose soil The initial 0.0m to 1.5m sample interval is drilled very slowly in order to achieve optimum sample recovery The entire 1.5m sample is collected at the drill rig in large numbered plastic bags for dispatch to the initial split preparation facility At the end of each drill rod, the drill string is cleaned by blowing down with air to remove any clay and silt potentially built up in the sample pipes The twin-tube aircore drilling technique is known to provide high quality samples from the face of the drill hole Wet and damp samples are placed into large plastic basins and exposed to the sun to dry prior to riffle splitting
Logging	*Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* *The total length and percentage of the relevant intersections logged.*	The 1.5m aircore samples were each qualitatively logged onto paper field sheets prior to digital entry into an Microsoft Excel spreadsheet The aircore samples were logged for lithology, colour, grainsize, rounding, sorting, estimated THM%, estimated Slimes% and any relevant comments - such as slope, vegetation, or cultural activity. Every drill hole was logged in full. Logging is undertaken with reference to a Drilling Guideline with codes prescribed and guidance on description to ensure consistent and systematic data collection
Sub-sampling techniques and sample preparation	*If core, whether cut or sawn and whether quarter, half or all core taken.* *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* *For all sample types, the nature, quality and appropriateness of the sample*	The entire 1.5m drill sample collected at the source was dispatched to a sample preparation facility to split with a riffle splitter to reduce sample size The water table depth was noted in all geological logs if intersected Samples with clay aggregates are gently hit with a rubber mallet to break them

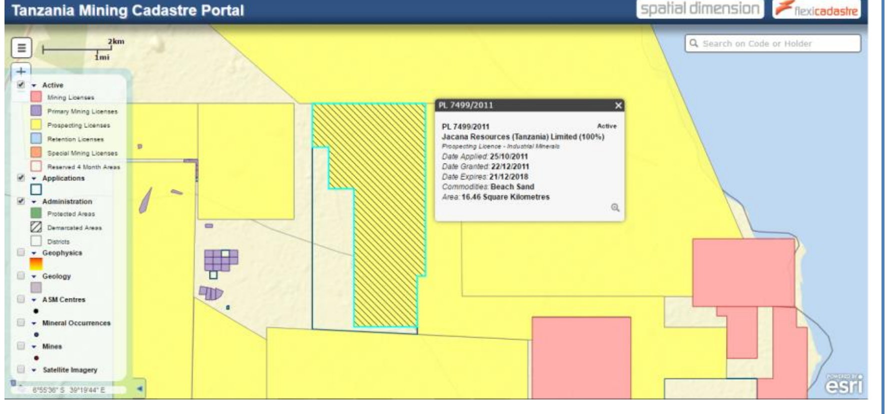
Criteria	JORC Code explanation	Commentary
	preparation technique. *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* *Whether sample sizes are appropriate to the grain size of the material being sampled.*	down so the sample with flow easily through the riffle splitter chutes A total of 1000 to 1300gm of each sample was inserted into calico sample bags and exported to Western Geolabs Laboratory for THM analysis Employees undertaking the splitting are closely monitored by a geologist to ensure sampling quality is maintained Almost all of the samples are sand, silty sand, sandy silt, clayey sand or sandy clay and this sample preparation method is considered appropriate The sample sizes were deemed suitable to reliably capture THM, slime, and oversize characteristics, based on industry experience of the geologists involved and consultation with laboratory staff Field duplicates of the samples were completed at a frequency of 1 per 50 primary samples Standard Reference Material samples are inserted into the sample stream in the field at a frequency of 1 per 50 samples. Overall this represents a QA/QC sample inserted at a rate of 1 per 25 samples. For Jacana drilling, the rate of submission for field duplicates was 1 in 36 and for the submission of blank samples (a replacement for standards) was also 1 in 36.
Quality of assay data and laboratory tests	*The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	The wet panning at the drill site provides an estimate of the THM% which is sufficient for the purpose of determining approximate concentrations of THM in the first instance Aircore sample: The individual 1.5m aircore sub-samples (approx. 1000gm) were assayed by Western Geolabs in Perth, Western Australia, which is considered the Primary laboratory The aircore samples were initially screened to +3mm to remove the very coarse sand, pebbles or grits. The remaining sample was split to 250g and it was screened for removal and determination of Slimes (-45µm) and Oversize (+1mm), then the sample was analysed for total heavy mineral (-1mm to +45µm) content by heavy liquid separation. The remaining sample – about 750g was retained for additional testwork The laboratory used TBE as the heavy liquid medium – with density range between 2.92 and 2.96 g/ml This is an industry standard technique Field duplicates of the samples were collected at a frequency of 1 per 50 primary samples

Criteria	JORC Code explanation	Commentary
		Western Geolabs completed its own internal QA/QC checks that included laboratory duplicates every 10th sample prior to the results being released Analysis of QA/QC samples show the laboratory data to be of acceptable accuracy and precision The density of the heavy liquid is checked daily or every time new or cleaned TBE was added for specific gravity using a hydrometer and volumetric flask. The adopted QA/QC protocols are acceptable for this stage of test work 1/40 samples from the Primary Laboratory have been sent to a Secondary Laboratory for check analysis and have been found to have very good repeatability for THM and Slimes.
Verification of sampling and assaying	*The verification of significant intersections by either independent or alternative company personnel.* *The use of twinned holes.* *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* *Discuss any adjustment to assay data.*	All results are checked by the companies Chief Geologist and Exploration Manager The company Chief Geologist and independent Resource geologist (Greg Jones) have made periodic visits to Western Geolabs to observe sample processing and procedure A process of laboratory data validation using mass balance is undertaken to identify entry errors or questionable data Field and laboratory duplicate data pairs (THM/oversize/slime) of each batch are plotted to identify potential quality control issues Standard Reference Material sample results are checked from each sample batch to ensure they are within tolerance (<2SD) and that there is no bias The field and laboratory data has been updated into a master spreadsheet which is appropriate for this stage in the programme. Data validation criteria are included to check for overlapping sample intervals, end of hole match between 'Lithology', 'Sample', 'Survey' files and other common errors A total of 36 twin holes were drilled in the programme. Of these twinned holes, one pair were both from the Jacana drilling, of the remaining 35, 4 were paired with Jacana holes that were not assayed and so were discarded for evaluation purposes. A total of 31 assayed twinned holes were used for comparative analysis. No adjustments were required to be made to the primary assay data No adjustments are made to the primary assay data
Location of data points	*Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* *Specification of the grid system used.*	Down hole surveys for shallow aircore holes are not required A handheld GPS was used to identify the positions of the drill holes in the field. The handheld GPS has an accuracy of +/- 10m in the horizontal The datum used is WGS84 and coordinates are projected as UTM zone 37S

Criteria	JORC Code explanation	Commentary
	Quality and adequacy of topographic control.	The drillhole collar elevation was collected from a detailed Digital Terrain Model collected in 2016. One metre contours were generated and the x-y coordinates were cut to the RL using the contour information. The accuracy of the locations is sufficient for this stage of exploration
Data spacing and distribution	*Data spacing for reporting of Exploration Results.* *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* *Whether sample compositing has been applied.*	A more regular square 100m x 50m grid spacing was achieved at Fungoni by infill drilling the previous offset drill grid of 100 x 100m Fungoni NW was drilled on a 200m x 50m spacing The tighter spaced aircore holes and regular grid are sufficient to provide a good degree of confidence in geological models and grade continuity within the holes Each aircore drill sample is a single 1.5m sample of sand intersected down the hole No compositing has been applied to models for values of THM, slime and oversize Compositing of samples was undertaken on HM concentrates for mineral assemblage determination. Composite samples were classified on geological domains
Orientation of data in relation to geological structure	*Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	The aircore drilling was oriented perpendicular to the strike of mineralization defined by previous drill data information The strike of the mineralization is sub-parallel to a slight topographic rise that appears to control the western contact of the mineralization. Drill holes were vertical and the orientation of the mineralisation is relatively horizontal The orientation of the drilling is considered appropriate for testing the lateral and vertical extent of mineralization without any bias
Sample security	*The measures taken to ensure sample security.*	Aircore samples remained in the custody of Company representatives while they were transported from the field to Dar es Salaam for final packaging and securing The samples were then sent using Deugro to Perth and delivered directly to the laboratory after quarantine inspection The laboratory inspected the packages and did not report tampering of the samples
Audits or reviews	*The results of any audits or reviews of sampling techniques and data.*	Internal reviews were undertaken

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	*Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* *The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.*	The exploration work was completed on tenements that are 100% owned by Strandline in Tanzania The drill samples for this Mineral Resource estimate were taken from tenement PL7499/2011 which owned 100% by Strandline Resources through its in country entity Jacana Resources The tenement is 4 years old and was recently reduced by 50% and is valid to 21 Dec. 2018 Traditional landowners and village Chiefs of the affected villages were supportive of the drilling programme 
Exploration done by other parties	*Acknowledgment and appraisal of exploration by other parties.*	Historic exploration work was completed by Tanganyika Gold in 1998 and 1999. OmegaCorp undertook reconnaissance exploration in 2005 and 2007 The Company has obtained the hardcopy reports and maps in relation to this information The historic data comprises surface sampling, limited auger drilling and mapping The historic results are not reportable under JORC 2012
Geology	*Deposit type, geological setting and style of mineralisation.*	Two types of heavy mineral placer style deposits are possible in Tanzania Thin but high grade strandlines which may be related to marine or fluvial influences Large but lower grade deposits related to windblown sands

Criteria	JORC Code explanation	Commentary
		The coastline of Tanzania is not well known for massive dunal systems such as those developed in Mozambique, however some dunes are known to occur and cannot be discounted as an exploration model. Palaeo strandlines are more likely and will be related to fossil shorelines or terraces in a marine or fluvial setting. In Tanzania three terraces have been documented and include the Mtoni terrace (1-5m ASL), Tanga (20-40m ASL) and Sakura Terrace (40 to 60m ASL). Strandline mineral sand accumulations related to massive storm events are thought to be preserved at these terraces above the current sea level.
Drill hole Information	*A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* *easting and northing of the drill hole collar* *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* *dip and azimuth of the hole* *down hole length and interception depth* *hole length.* *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	The drill hole data are reported as composited intervals at greater than 1 per cent THM and presented in **Appendix 2**
Data aggregation methods	*In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	No data aggregation methods were utilised on the THM grades, no top cuts were employed and all cut-off grades have been reported There was data aggregation of altered ilmenite and ilmenite to one mineral grouping of Ilmenite in order for the SEM_EDX mineral assemblage method to be incorporated with the magnetic separation mineral assemblage method used at Fungoni NW
Relationship between mineralisation widths and intercept lengths	*These relationships are particularly important in the reporting of Exploration Results.* *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	The nature of the mineralisation is broadly horizontal, thus vertical aircore holes are thought to represent close to true thicknesses of the mineralisation Downhole widths are reported
Diagrams	*Appropriate maps and sections (with scales) and tabulations of intercepts*	Figures and plans are displayed in the main text of the Release

Criteria	JORC Code explanation	Commentary
	should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	
Balanced reporting	*Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	All results > 1.0% THM have been reported as average composite lengths **– refer to Appendix 2**
Other substantive exploration data	*Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Detailed mineral assemblage work was undertaken on composite samples for Fungoni by Process Mineralogical Consulting Ltd (PMC) and by Allied Mineral Laboratories (AML) **(refer to Appendix 3).** The preparation of the composites prior to physical separation or assaying is described as: • Detailed sachet scanning of heavy mineral sinks from the drill assay process was carried out to determine regions of gross mineralogy as well as an overall consideration of valuable heavy mineral (VHM) content. Other considerations undertaken during this sachet logging were the presence of iron oxide coatings on THM, and any gross composition of trash HM. • Sachet scanning then formed the input to the geological / mineralogical / THM grade interpretation which was then used to drive domain control for modelling, as well as providing the guidance for the allocation of mineral assemblage composites. • Three individual domains were identified for the purpose of guiding the allocation of composites; the upper zone (ZONE=2), the oxide zone (ZONE=4) and the lower zone (ZONE=5). These domains were further subdivided into north-south sample regions, with each mineral assemblage composite collected from two drill lines approximately 100 m apart (refer Figure 10) - with the exception of the southernmost three lines that were composited together. • For the north-west extension of Fungoni where drilling was spaced at 200 m spaced drill lines and the morphology of strands was shallower and narrower than the main deposit, the selection of composites was made over 3 drill lines. In the case of the lower domain (ZONE=5) the entire domain north of 17200 mN was composited together. This approach was taken for the north-west extension due to the smaller weight of material available to prepare composites for the selected mineralogy determination

Criteria	JORC Code explanation	Commentary
		method. • A total of 22 mineral assemblage composites were used to characterise the mineralogy and chemistry for the main Fungoni project and a further 5 composites were used to characterise the north-west extension. • Individual drill hole samples were selected based on whether they fell within a particular domain, and were then proportioned against contained THM grade in order to specify the weight of THM that each sample would contribute to the entire composite. • Once all of the ratio calculations were completed, the spreadsheet with sample identification and mineral assemblage composite number was submitted to Geoff Lane at Process Mineralogical Consulting Ltd (PMC) in Canada for sample collation and processing for the main Fungoni deposit, and for the north-west extension, the samples were sent to Allied Mineral Laboratory (AML) in Perth. • Preparing the mineral assemblage composites in this manner allows for composite results to be applied to the resource block model and for those results to then be reported and weighted on THM in the final Mineral Resource estimate. • Details of mineral assemblage composite IDs with associated results are presented in Appendix 3 The method of analysis by PMC for the main Fungoni deposit was by a Scanning Electron Microscope (Tescan Vega 3) fitted with an Energy Dispersive Spectrometer (SEM-EDS) and equipped with Tescan Integrated Mineral Analyser (TIMA) and Oxford INCA Feature software capable of searching and quantifying the elemental composition of a statistically representative number of Ti-species including rutile, ilmenite, Ti-magnetite, pseudo-rutile and leucoxene. Mineral assemblage and characterisation comprise: • Composite Samples were reduced with a micro riffle splitter to approximately 2-5 g for preparation of a polished section • Total oxide geochemistry on a grain-by-grain basis

Criteria	JORC Code explanation	Commentary
		• Mineral species determination by chemical analysis • Mineral species mass % calculated from the grain spherical volume (derived from exposed grain surface area) multiplied by the mineral density • Approximately 2000-3000 grain counts, sizing and probing for mineral chemistry analysis for each sample • Titanium deportment for each titanium species • Zircon – total oxide mineral geochemistry for zircon analysis A separate sub-sample of each was analysed by standard XRF techniques to ensure quality control of the SEM analysis by comparing actual XRF whole rock analysis with the SEM calculated whole rock analysis for each sample The SEM-EDX method provides detailed grain chemistry in conjunction with a modal mineral mass balance to 100%. The method is constrained when the heavy mineral is coarse grained and the XRF (X-Ray Fluorescence) determination is required to assist in allocating modal mineral abundances. The mineral assemblage composites from the north-west extension of Fungoni were assayed by magnetic separation into 3 fractions, magnetic, para-magnetic and non-magnetic. These fractions were then assayed by XRF to determine oxide grades. The ratio and relationship of specific oxides to mineral species and their deportment based on magnetic properties can be used to back calculate overall mineral mass distribution. The results of this method are in alignment with the SEM-EDX results, without the specific mineral breakdown for magnetic and non-magnetic trash mineral species. In order to report the two data set methodologies, some aggregation of the SEM-EDX mineralogy was required. For transparency the two data sets are shown in Appendix 3.
Further work	*The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Additional work is planned for the determination of bulk density and insitu density, as well as standard penetration testing to determine sand properties. Metallurgical testwork is ongoing

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	*Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.* *Data validation procedures used.*	Original laboratory files used to populate exploration database assay tables via an automatic software assay importer where available. Checks of data by visually inspecting on screen (to identify translation of samples), duplicate and twin drilling was visually examined to check the reproducibility of assays. Database assay values have been subjected to random reconciliation with laboratory certified value is to ensure agreement. Visual and statistical comparison was undertaken to check the validity of results
Site visits	*Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* *If no site visits have been undertaken indicate why this is the case.*	Regular site trips before and during the resource drilling phase were undertaken by Brendan Cummins. Mr Cummins was onsite between the 27^{th} July until 6^{th} August 2016 to observe the drilling and data collection activities
Geological interpretation	*Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* *Nature of the data used and of any assumptions made.* *The effect, if any, of alternative interpretations on Mineral Resource estimation.* *The use of geology in guiding and controlling Mineral Resource estimation.* *The factors affecting continuity both of grade and geology.*	The geological interpretation was undertaken by Brendan Cummins and data was used by Greg Jones and then validated using all logging and sampling data and observations. Current data spacing and quality is sufficient to indicate grade continuity. The possibility of narrow washouts between drill lines exists but they are not considered likely given the depositional environment. Interpretation of modelling domains was restricted to the main mineralised envelopes utilising THM sinks, slimes, trash mineralogy and geology logging. No other interpretations were considered as the Competent Person was satisfied that the sachet logging which was used to define the mineral assemblage composites was effective in outlining the major mineralogical domains. This is the primary objective for any mineral sands resource estimation. The Mineral Resource estimate was controlled to an extent by the geological envelope and basement surfaces. The mineralisation for Fungoni has either been truncated at surface by erosion of the original deposit, or there has been a combination of erosion and concentration of heavy mineral and particular VHM close to surface.
Dimensions	*The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The Mineral Resource for Fungoni is approximately 2 km long and 850 m wide on average. The deposit ranges in thickness from approximately 2 to 13 m.

Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	*The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* *The assumptions made regarding recovery of by-products.* *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).* *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* *Any assumptions behind modelling of selective mining units.* *Any assumptions about correlation between variables.* *Description of how the geological interpretation was used to control the resource estimates.* *Discussion of basis for using or not using grade cutting or capping.* *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	The mineral resource estimate was conducted using CAE mining software (also known as Datamine Studio). Inverse distance weighting techniques were used to interpolate assay grades from drill hole samples into the block model and nearest neighbour techniques were used to interpolate index values and nonnumeric sample identification into the block model. The mostly regular dimensions of the drill grid and the anisotropy of the drilling and sampling grid allowed for the use of inverse distance methodologies as no de-clustering of samples was required. Appropriate and industry standard search ellipses were used to search for data for the interpolation and suitable limitations on the number of samples and the impact of those samples was maintained. An inverse distance weighting power of 3 was used so as not to over smooth the grade interpolations. Hard domain boundaries were used and these were defined by the geological wireframes that were interpreted. This Mineral Resource estimate for the Fungoni main deposit compares well with the previous resource prepared by AMC and reported by Jacana in 2013. There are differences in domain control, reporting of predominantly upper zone material and final JORC Classification that makes it difficult to reconcile directly between the 2 resource estimates. However the material being reported in the Measured and Indicated categories for this 2017 resource estimate would equate to that material being reported as part of the Indicated resource estimate previously. No assumptions were made during the resource estimation as to the recovery of byproducts. Slimes and oversize contents are estimated at the same time as estimating the THM grade. Further detailed geochemistry is required to ascertain deleterious elements that may affect the marketability of the heavy mineral products The average parent cell size used for the interpolation was approximately half the standard drill hole width and a half the standard drill hole section line spacing. Given that the average drill hole spacing for Fungoni was 50 m east-west and 100 m north south and with 1.5 m samples the parent cell size was 25 x 50 x 1.5 m (where the Z or vertical direction of the cell was nominated as the same distance as the sample length). No assumptions were made regarding the modelling of selective mining units however it is assumed that a form of dry mining will be undertaken and the cell size and the sub cell splitting will allow for an appropriate dry mining preliminary reserve to be prepared. Any other mining methodology will be

Criteria	JORC Code explanation	Commentary
		more than adequately catered for with the parent cell size that was selected for the modelling exercise. No assumptions were made about correlation between variables. The Mineral Resource estimates were controlled to an extent by the geological / mineralisation and basement surfaces. Grade cutting or capping was not used during the interpolation because of the regular nature of sample spacing and the fact that samples were not clustered nor wide spaced to an extent where elevated samples could have a deleterious impact on the resource estimation. Sample distributions were reviewed and no extreme outliers were identified either high or low that necessitated any grade cutting or capping. The sample length of 1.5 m does result in a degree of grade smoothing also negating the requirement for grade cutting or capping. Validation of grade interpolations were done visually In CAE Studio (Datamine) software by loading model and drill hole files and annotating and colouring and using filtering to check for the appropriateness of interpolations. Statistical distributions were prepared for model zones from drill hole and model files to compare the effectiveness of the interpolation. Along strike distributions of section line averages (swath plots) for drill holes and models were also prepared for comparison purposes.
Moisture	*Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Tonnages were estimated an assumed dry basis. A bulk density conversion factor was used as per the previous Mineral Resource estimate prepared by AMC. This factor is 1.80 g/cm^3 and based on the experience of the Competent Person. We believe the bulk density conversion factor to be appropriate at this level of confidence for the Mineral Resource estimates based on our experience and we would also recommend that bulk density testwork be undertaken going forward.
Cut-off parameters	*The basis of the adopted cut-off grade(s) or quality parameters applied.*	Cut-off grades for HM and SLIMES as well as hardness were used to prepare the reported resource estimates. These cut-off grades were defined by the Competent Person as being based soundly on experience, the percentage of VHM and the grade tonnage curves taken in consideration with the grade distribution along the length of the deposits.
Mining factors or assumptions	*Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating*	No specific mining method is assumed other than potentially the use of dry mining scrapers and excavators into trucks. This allows for quite a selective mining process while still maintaining bulk economies of scale as the dark HM at the base of the orebody allows for excellent visual acuity and therefore grade control. To this end no minimum thickness was assumed for the

Criteria	JORC Code explanation	Commentary
	Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	reporting of the mineral resource.
Metallurgical factors or assumptions	*The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Metallurgical assumptions were used based on mineral assemblage composites which at this stage only allow for preliminary commentary with no final products being defined from the reported mineral species. Some chemistry in the form of oxides from XRF analysis was available for commentary however may not bear exact reconciliation with eventual final products.
Environmental factors or assumptions	*Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	No assumptions have been made regarding possible waste and process residue however disposal of byproducts such as SLIMES, sand and oversize are normally part of capture and disposal back into the mining void for eventual rehabilitation. This also applies to mineral products recovered and waste products recovered from metallurgical processing of heavy mineral.
Bulk density	*Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	A bulk density conversion factor was used as per a previous Mineral Resource estimate prepared by AMC. This factor is 1.80 g/cm^3 and based on the experience of the Competent Person. We believe the bulk density conversion factor to be appropriate at this level of confidence for the Mineral Resource estimates based on our experience and we would also recommend that bulk density testwork be undertaken going forward.
Classification	*The basis for the classification of the Mineral Resources into varying confidence categories.* *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The resource classification for the Fungoni deposit was based on the following criteria: drill hole spacing, geological and grade continuity, variography of primary assay grades and the distribution of bulk samples. The classification of the Measured and Indicated Resources was supported by all of the supporting criteria as noted above. As a Competent Person, IHC Robbins Resource & Business Development Manager Greg Jones considers that the result appropriately reflects a reasonable view of the deposit categorisation.

Criteria	JORC Code explanation	Commentary
Audits or reviews	*The results of any audits or reviews of Mineral Resource estimates.*	No audits or reviews of the mineral resource estimate have been undertaken but Mining Consultants advising the Company will be undertaking their own review as part of the Feasibility study
Discussion of relative accuracy/ confidence	*Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	There was an evaluative geostatistical process undertaken (variography supporting ordinary Kriging) during the resource estimation of the Fungoni deposit. The overall grade interpolation was a fair comparison with inverse distance weighting methodology, however had a tendency to over smooth high grade and low grade areas. For this reason it was decided to use the inverse distance weighting interpolation methodology as it also had the best correlation/comparison with the drill hole grades. Validation of the model vs drill hole grades by observation, swathe plot and population distribution analysis was favourable The statement refers to global estimates for the entire known extent of the Fungoni deposit. No production data is available for comparison with the Fungoni deposit.

Appendix 2: Downhole Average Drill Intersects

Fungoni > 1% THM drill intersects from Fungoni and Fungoni NW

HOLE ID	EASTING	NORTHING	RL	AZIMUTH	DIP	EOH	FROM	TO	LENGTH	THM	SLIMES	OS +1mm	OS +3mm
	WGS84 ZONE 37S	WGS84 ZONE 37S	(m)			(m)	(m)	(m)	(m)	%	%	%	%
CSAC0004	548055.44	9225807.00	39.63	0	90	48	2	4	2	1.4	13.8	2.3	0.0
CSAC0004	548055.44	9225807.00	35.63	0	90	48	6	8	2	1.2	17.5	3.5	0.0
CSAC0005	547973.00	9225785.00	36.00	0	90	40	0	12	12	2.4	21.4	5.3	0.0
CSAC0005	547973.00	9225785.00	3.00	0	90	40	38	40	2	1.5	10.4	2.0	0.0
CSAC0007	548153.31	9226294.00	36.98	0	90	66	0	10	10	12.7	24.9	11.4	0.0
CSAC0007	548153.31	9226294.00	12.98	0	90	66	28	30	2	1.2	57.0	16.2	0.0
CSAC0007	548153.31	9226294.00	0.98	0	90	66	36	46	10	1.7	27.1	4.1	0.0
CSAC0007	548153.31	9226294.00	-9.02	0	90	66	48	54	6	1.8	15.6	8.2	0.0
CSAC0007	548153.31	9226294.00	-23.02	0	90	66	64	66	2	1.2	20.2	1.6	0.0
CSAC0008	548203.13	9226302.00	35.59	0	90	75	0	12	12	6.5	33.5	7.9	0.0
CSAC0008	548203.13	9226302.00	20.59	0	90	75	18	24	6	1.3	17.8	7.6	0.0
CSAC0008	548203.13	9226302.00	-3.41	0	90	75	44	46	2	1.1	7.5	3.3	0.0
CSAC0008	548203.13	9226302.00	-11.41	0	90	75	50	56	6	1.1	21.9	9.9	0.0
CSAC0009	548298.94	9226299.00	37.40	0	90	52	0	8	8	4.1	25.8	4.7	0.0
CSAC0009	548298.94	9226299.00	10.40	0	90	52	30	32	2	1.5	10.2	7.3	0.0
CSAC0010	548000.25	9226301.00	40.00	0	90	68	0	4	4	5.1	17.2	2.2	0.0
CSAC0010	548000.25	9226301.00	25.00	0	90	68	12	22	10	1.3	32.5	12.3	0.0
CSAC0010	548000.25	9226301.00	17.00	0	90	68	24	26	2	1.2	40.2	2.9	0.0
CSAC0010	548000.25	9226301.00	13.00	0	90	68	28	30	2	1.1	49.6	3.9	0.0
CSAC0010	548000.25	9226301.00	5.00	0	90	68	36	38	2	1.0	32.5	10.8	0.0
CSAC0010	548000.25	9226301.00	-1.00	0	90	68	42	44	2	1.8	29.7	10.1	0.0
CSAC0010	548000.25	9226301.00	-15.00	0	90	68	48	66	18	1.9	24.5	13.2	0.0
CSAC0014	548293.25	9226493.00	39.40	0	90	26	0	2	2	2.4	11.5	3.2	0.0
CSAC0014	548293.25	9226493.00	31.40	0	90	26	8	10	2	1.5	52.0	8.7	0.0
CSAC0015	548199.50	9226500.00	37.97	0	90	36	0	6	6	11.5	23.6	9.0	0.0
CSAC0015	548199.50	9226500.00	22.97	0	90	36	16	20	4	1.3	26.9	8.9	0.0
CSAC0015	548199.50	9226500.00	15.97	0	90	36	24	26	2	1.9	25.3	8.5	0.0
CSAC0016	548095.31	9226503.00	32.42	0	90	44	0	20	20	6.6	29.7	8.2	0.0
CSAC0016	548095.31	9226503.00	2.42	0	90	44	36	44	8	1.4	25.9	19.7	0.0
CSAC0017	547897.25	9226498.00	41.99	0	90	33	0	8	8	4.7	29.7	3.7	0.0
CSAC0017	547897.25	9226498.00	26.99	0	90	33	12	26	14	1.9	33.7	10.8	0.0
CSAC0017	547897.25	9226498.00	14.49	0	90	33	30	33	3	1.7	28.3	14.8	0.0
CSAC0019	548101.94	9226700.00	37.57	0	90	44	0	8	8	7.9	30.8	8.3	0.0
CSAC0019	548101.94	9226700.00	24.57	0	90	44	16	18	2	1.2	43.1	21.5	0.0
CSAC0019	548101.94	9226700.00	20.57	0	90	44	20	22	2	1.2	23.6	7.4	0.0
CSAC0019	548101.94	9226700.00	7.57	0	90	44	32	36	4	2.5	31.2	5.7	0.0
CSAC0019	548101.94	9226700.00	2.57	0	90	44	38	40	2	1.0	16.9	9.0	0.0
CSAC0019	548101.94	9226700.00	-1.43	0	90	44	42	44	2	1.6	29.8	6.8	0.0

CSAC0020	548102.50	9226102.00	37.00	0	90	33	0	10	10	6.1	25.2	11.1	0.0
CSAC0020	548102.50	9226102.00	12.00	0	90	33	28	32	4	1.5	29.8	3.8	0.0
CSAC0021	548202.44	9226102.00	37.00	0	90	28	0	10	10	3.9	22.3	8.0	0.0
CSAC0022	548001.31	9226694.00	44.45	0	90	32	0	2	2	1.3	26.0	7.3	0.0
CSAC0022	548001.31	9226694.00	40.45	0	90	32	4	6	2	1.8	27.3	7.8	0.0
CSAC0022	548001.31	9226694.00	34.45	0	90	32	10	12	2	1.0	23.9	1.3	0.0
CSAC0022	548001.31	9226694.00	16.45	0	90	32	26	32	6	1.2	28.2	20.9	0.0
CSAC0023	547905.94	9226703.00	49.00	0	90	28	0	2	2	1.2	27.5	2.3	0.0
CSAC0023	547905.94	9226703.00	29.00	0	90	28	20	22	2	1.1	32.8	2.8	0.0
CSAC0024	548304.50	9226698.00	35.00	0	90	24	4	6	2	1.1	17.8	12.0	2.1
CSAC0024	548304.50	9226698.00	29.00	0	90	24	8	14	6	2.6	13.1	9.4	0.2
CSAC0028	548050.56	9226595.00	39.47	0	90	26	0	6	6	5.5	34.8	5.8	0.0
CSAC0028	548050.56	9226595.00	25.47	0	90	26	16	18	2	1.1	37.8	26.1	0.0
CSAC0029	548146.38	9226596.00	37.43	0	90	34	0	8	8	16.3	25.3	9.1	0.0
CSAC0029	548146.38	9226596.00	30.43	0	90	34	10	12	2	1.8	26.7	4.1	0.0
CSAC0029	548146.38	9226596.00	23.43	0	90	34	14	22	8	1.2	28.9	8.2	0.0
CSAC0029	548146.38	9226596.00	16.43	0	90	34	24	26	2	1.3	30.6	9.1	0.0
CSAC0030	547963.19	9226597.00	42.08	0	90	18	0	6	6	1.5	13.2	3.3	0.0
CSAC0031	547853.00	9226396.00	29.80	0	90	18	14	16	2	1.2	34.5	16.9	0.0
CSAC0032	547949.38	9226397.00	40.00	0	90	24	0	4	4	4.0	18.4	3.2	0.0
CSAC0032	547949.38	9226397.00	21.00	0	90	24	18	24	6	1.6	32.4	12.4	0.0
CSAC0033	548049.81	9226395.00	37.00	0	90	38	0	10	10	6.7	25.9	8.1	0.0
CSAC0033	548049.81	9226395.00	25.00	0	90	38	12	22	10	1.6	33.6	12.3	0.0
CSAC0033	548049.81	9226395.00	17.00	0	90	38	24	26	2	1.6	37.6	2.9	0.0
CSAC0033	548049.81	9226395.00	9.00	0	90	38	32	34	2	1.0	34.7	6.6	0.0
CSAC0034	548145.81	9226394.00	35.49	0	90	30	0	12	12	7.4	25.9	7.3	0.0
CSAC0035	548245.81	9226397.00	38.00	0	90	18	0	6	6	6.8	28.7	12.4	0.0
CSAC0038	548349.00	9226201.00	40.61	0	90	18	0	2	2	1.1	6.5	3.5	0.0
CSAC0039	548250.75	9226204.00	37.00	0	90	30	0	10	10	3.6	21.7	7.6	0.0
CSAC0040	548151.25	9226202.00	34.00	0	90	42	0	16	16	9.4	25.9	10.9	0.0
CSAC0040	548151.25	9226202.00	9.00	0	90	42	32	34	2	1.2	35.8	9.9	0.0
CSAC0041	548052.63	9226202.00	38.00	0	90	24	0	8	8	9.5	24.8	9.9	0.0
CSAC0041	548052.63	9226202.00	31.00	0	90	24	10	12	2	1.1	40.4	5.3	0.0
CSAC0042	547954.25	9226199.00	41.00	0	90	20	0	2	2	4.1	4.4	2.3	0.0
CSAC0042	547954.25	9226199.00	35.00	0	90	20	6	8	2	4.6	14.8	3.6	0.0
CSAC0042	547954.25	9226199.00	26.00	0	90	20	12	20	8	1.3	31.9	9.6	0.0
CSAC0043	547800.25	9226102.00	19.05	0	90	30	20	26	6	1.8	35.2	22.6	0.0
CSAC0044	547898.25	9226098.00	39.00	0	90	30	0	6	6	1.4	24.3	7.9	0.0
CSAC0044	547898.25	9226098.00	15.00	0	90	30	24	30	6	1.4	24.9	5.3	0.0
CSAC0045	548009.13	9226114.00	40.00	0	90	32	0	4	4	5.7	11.7	3.1	0.0
CSAC0045	548009.13	9226114.00	35.00	0	90	32	6	8	2	1.0	29.0	5.5	0.0
CSAC0045	548009.13	9226114.00	31.00	0	90	32	10	12	2	1.1	33.8	6.6	0.0
CSAC0045	548009.13	9226114.00	13.00	0	90	32	28	30	2	1.2	22.7	12.1	0.0

CSAC0046	548297.69	9226101.00	40.00	0	90	18	0	4	4	1.5	7.3	4.6	0.0
CSAC0049	548249.94	9226002.00	40.55	0	90	26	0	4	4	1.1	6.3	1.5	0.0
CSAC0050	548142.81	9226002.00	35.00	0	90	36	0	14	14	3.4	20.5	5.7	0.0
CSAC0051	548057.56	9226016.00	39.00	0	90	30	0	6	6	4.4	19.1	8.6	0.0
CSAC0051	548057.56	9226016.00	27.00	0	90	30	14	16	2	1.4	30.9	15.3	0.0
CSAC0052	547842.94	9226005.00	41.00	0	90	32	0	2	2	1.2	6.9	5.4	0.0
CSAC0052	547842.94	9226005.00	21.00	0	90	32	16	26	10	2.2	33.5	16.2	0.0
CSAC0053	547892.25	9225902.00	40.00	0	90	36	0	4	4	2.7	13.8	3.4	0.0
CSAC0053	547892.25	9225902.00	28.00	0	90	36	12	16	4	1.3	39.7	20.9	0.0
CSAC0053	547892.25	9225902.00	15.00	0	90	36	26	28	2	2.0	36.4	5.9	0.0
CSAC0054	547997.94	9225903.00	36.00	0	90	30	0	12	12	2.9	21.7	5.4	0.0
CSAC0054	547997.94	9225903.00	19.00	0	90	30	20	26	6	1.1	22.3	8.7	0.0
CSAC0055	548104.25	9225906.00	35.62	0	90	30	0	14	14	3.1	20.2	4.8	0.0
CSAC0058	547797.50	9226701.00	47.00	0	90	32	0	6	6	1.8	22.7	6.5	0.1
CSAC0058	547797.50	9226701.00	35.00	0	90	32	14	16	2	1.0	48.0	3.2	0.0
CSAC0059	547851.19	9226605.00	48.05	0	90	26	0	4	4	1.4	24.4	5.0	0.0
CSAC0060	547851.88	9226804.00	48.00	0	90	18	0	4	4	1.6	23.1	3.6	0.1
CSAC0060	547851.88	9226804.00	35.00	0	90	18	14	16	2	1.4	34.8	1.3	0.0
CSAC0061	547951.19	9226801.00	46.70	0	90	20	0	6	6	2.5	30.5	28.9	0.0
CSAC0062	548060.75	9226803.00	37.67	0	90	30	0	12	12	6.0	30.6	9.1	0.0
CSAC0062	548060.75	9226803.00	20.67	0	90	30	22	24	2	1.1	39.2	13.6	0.0
CSAC0062	548060.75	9226803.00	16.67	0	90	30	26	28	2	1.0	31.8	9.4	0.0
CSAC0063	548114.50	9226805.00	38.84	0	90	30	0	4	4	9.4	19.8	5.4	0.0
CSAC0063	548114.50	9226805.00	33.84	0	90	30	6	8	2	1.7	29.5	5.7	0.0
CSAC0063	548114.50	9226805.00	22.84	0	90	30	16	20	4	1.2	34.6	12.6	0.0
CSAC0064	548099.94	9226300.00	35.00	0	90	30	0	14	14	6.6	26.7	6.2	0.0
CSAC0064	548099.94	9226300.00	13.00	0	90	30	28	30	2	1.0	26.0	3.2	0.0
CSAC0065	547699.88	9226102.00	40.44	0	90	24	0	8	8	2.9	13.0	6.3	0.1
CSAC0066	547650.56	9226002.00	43.84	0	90	20	0	2	2	1.2	3.7	9.3	0.3
CSAC0066	547650.56	9226002.00	34.84	0	90	20	8	12	4	1.1	16.8	13.5	0.5
CSAC0068	547744.94	9226010.00	39.18	0	90	24	2	4	2	2.1	24.8	3.3	0.0
CSAC0068	547744.94	9226010.00	19.18	0	90	24	22	24	2	1.2	32.1	11.1	0.0
CSAC0069	547799.13	9225905.00	40.00	0	90	48	0	4	4	3.1	17.6	7.6	0.0
CSAC0069	547799.13	9225905.00	19.00	0	90	48	16	30	14	2.0	31.6	15.4	0.0
CSAC0069	547799.13	9225905.00	-1.00	0	90	48	40	46	6	1.4	29.0	8.4	0.0
CSAC0070	548003.13	9225698.00	38.00	0	90	28	0	10	10	1.8	11.7	5.0	0.4
CSAC0071	547904.75	9225699.00	38.06	0	90	40	0	8	8	2.4	17.0	4.7	0.0
CSAC0071	547904.75	9225699.00	29.06	0	90	40	10	16	6	1.4	33.5	3.5	0.0
CSAC0072	547808.00	9225693.00	38.00	0	90	30	0	8	8	2.1	29.8	6.4	0.0
CSAC0072	547808.00	9225693.00	27.00	0	90	30	14	16	2	1.4	27.0	11.8	0.0
CSAC0077	547801.75	9226501.00	39.23	0	90	34	8	14	6	1.6	29.8	10.4	0.5
CSAC0079	548352.69	9226802.00	35.00	0	90	30	4	6	2	1.1	23.0	6.6	0.3
CSAC0079	548352.69	9226802.00	30.00	0	90	30	8	12	4	2.7	11.6	31.3	3.0

CSAC0079	548352.69	9226802.00	25.00	0	90	30	14	16	2	1.8	19.2	5.7	0.1
CSAC0080	548251.94	9226805.00	28.00	0	90	28	8	16	8	1.4	18.8	11.1	0.1
CSAC0081	548216.25	9226880.00	28.22	0	90	30	10	12	2	1.3	26.8	7.1	0.9
CSAC0084	547554.75	9225800.00	46.27	0	90	18	0	4	4	1.2	29.9	8.4	0.0
CSAC0084	547554.75	9225800.00	35.27	0	90	18	12	14	2	1.0	36.8	4.6	0.0
CSAC0084	547554.75	9225800.00	31.27	0	90	18	16	18	2	1.4	29.5	4.2	0.0
CSAC0085	547602.56	9225701.00	41.08	0	90	46	0	6	6	2.6	16.7	7.5	0.0
CSAC0085	547602.56	9225701.00	19.08	0	90	46	24	26	2	1.0	40.6	8.2	0.0
CSAC0085	547602.56	9225701.00	15.08	0	90	46	28	30	2	1.1	38.5	26.1	0.0
CSAC0085	547602.56	9225701.00	4.08	0	90	46	34	46	12	1.6	36.2	16.1	0.0
CSAC0086	547649.38	9225600.00	41.29	0	90	28	0	6	6	2.5	21.1	10.2	0.0
CSAC0086	547649.38	9225600.00	23.29	0	90	28	20	22	2	1.2	31.1	8.6	0.0
CSAC0086	547649.38	9225600.00	18.29	0	90	28	24	28	4	1.4	34.8	8.1	0.0
CSAC0087	547748.19	9225602.00	40.00	0	90	28	0	4	4	3.6	11.6	2.3	0.0
CSAC0087	547748.19	9225602.00	35.00	0	90	28	6	8	2	2.4	29.5	7.3	0.0
CSAC0093	547905.69	9225502.00	37.91	0	90	22	4	6	2	1.1	4.2	3.4	0.0
CSAC0094	547953.69	9225600.00	30.00	0	90	28	10	16	6	1.5	28.8	7.6	0.7
CSAC0095	547853.13	9225606.00	40.00	0	90	32	0	4	4	2.9	8.4	1.8	0.0
CSAC0095	547853.13	9225606.00	27.00	0	90	32	12	18	6	1.4	41.5	3.8	0.0
CSAC0095	547853.13	9225606.00	14.00	0	90	32	26	30	4	1.1	31.1	3.8	0.0
CSAC0096	547800.38	9225503.00	39.00	0	90	24	0	6	6	2.1	10.6	3.5	0.0
CSAC0096	547800.38	9225503.00	29.00	0	90	24	12	14	2	1.5	30.3	16.2	0.0
CSAC0097	547700.75	9225503.00	40.13	0	90	30	0	6	6	2.2	20.9	7.3	0.0
CSAC0097	547700.75	9225503.00	28.13	0	90	30	8	22	14	1.7	39.1	15.8	0.0
CSAC0098	547601.38	9225503.00	41.59	0	90	30	2	8	6	1.5	20.2	6.6	0.0
CSAC0100	547549.63	9225599.00	45.68	0	90	18	2	4	2	1.0	17.7	4.8	0.0
CSAC0100	547549.63	9225599.00	39.68	0	90	18	8	10	2	2.1	25.0	5.6	0.0
CSAC0103	547684.38	9225699.00	39.00	0	90	32	2	4	2	1.0	29.2	7.4	0.0
CSAC0103	547684.38	9225699.00	22.00	0	90	32	18	22	4	1.4	33.2	29.2	0.0
CSAC0114	547852.88	9226200.00	18.00	0	90	56	18	30	12	2.1	32.6	14.4	0.0
CSAC0114	547852.88	9226200.00	-4.00	0	90	56	42	50	8	3.3	20.0	4.8	0.0
CSAC0126	547650.50	9225404.00	40.88	0	90	44	0	4	4	2.4	12.0	5.4	0.0
CSAC0126	547650.50	9225404.00	27.88	0	90	44	14	16	2	1.2	41.9	10.8	0.0
CSAC0126	547650.50	9225404.00	19.88	0	90	44	18	28	10	1.7	28.0	13.8	0.0
CSAC0127	547752.13	9225404.00	40.00	0	90	34	0	4	4	2.0	8.3	0.9	0.0
CSAC0127	547752.13	9225404.00	32.00	0	90	34	8	12	4	1.2	36.0	5.4	0.0
CSAC0127	547752.13	9225404.00	26.00	0	90	34	14	18	4	2.1	26.6	12.8	0.0
CSAC0128	547852.94	9225397.00	37.21	0	90	40	4	6	2	1.2	9.3	4.6	0.0
CSAC0128	547852.94	9225397.00	16.21	0	90	40	24	28	4	1.1	26.6	11.0	0.0
CSAC0134	547598.44	9226102.00	46.20	0	90	30	0	4	4	1.7	8.2	13.7	0.6
CSAC0135	547750.69	9226201.00	41.95	0	90	36	0	6	6	1.5	7.4	5.3	0.0
CSAC0166	547738.13	9225209.00	37.71	0	90	22	2	6	4	1.2	5.7	6.9	0.2
CSAC0166	547738.13	9225209.00	27.71	0	90	22	12	16	4	2.3	21.8	17.2	1.3

CSAC0169	547550.13	9225204.00	40.58	0	90	30	0	6	6	1.6	8.0	8.9	0.3
CSAC0169	547550.13	9225204.00	30.58	0	90	30	12	14	2	1.2	14.0	17.3	1.9
CSAC0170	547450.00	9225203.00	45.51	0	90	30	0	8	8	3.3	21.4	4.9	0.0
CSAC0171	547501.13	9225137.00	41.66	0	90	30	0	6	6	2.8	7.0	7.4	0.0
CSAC0171	547501.13	9225137.00	31.66	0	90	30	12	14	2	1.0	66.8	3.8	0.0
CSAC0172	547495.19	9225307.00	43.99	0	90	30	0	8	8	1.7	15.6	6.7	0.0
CSAC0192	547597.56	9225902.00	33.87	0	90	28	12	14	2	1.2	34.1	4.0	0.0
CSAC0192	547597.56	9225902.00	29.87	0	90	28	16	18	2	1.4	24.9	7.5	0.0
CSAC0192	547597.56	9225902.00	22.87	0	90	28	20	28	8	1.7	47.6	8.2	0.0
CSAC0202	548047.63	9227004.00	44.72	0	90	40	0	6	6	5.3	15.5	8.2	0.2
CSAC0202	548047.63	9227004.00	38.72	0	90	40	8	10	2	1.1	30.0	2.7	0.2
CSAC0203	547949.88	9227005.00	48.23	0	90	44	0	2	2	1.7	19.2	4.9	0.0
CSAC0204	548000.38	9226902.00	46.22	0	90	40	0	6	6	2.6	25.4	5.0	0.0
CSAC0204	548000.38	9226902.00	14.22	0	90	40	30	40	10	1.6	26.3	7.2	0.0
CSAC0210	547855.88	9227006.00	45.52	0	90	40	0	8	8	4.4	22.6	7.6	0.4
CSAC0211	547999.13	9227103.00	45.65	0	90	38	0	4	4	1.5	14.9	12.7	0.3
CSAC0218	547804.56	9226902.00	47.00	0	90	40	0	6	6	1.6	25.6	6.0	0.0
16FGAC295	548048.94	9227100.00	44.88	0	90	12	0	4.5	4.5	2.3	13.7	5.2	0.3
16FGAC296	547997.63	9227100.00	46.20	0	90	12	0	3	3	1.4	10.8	8.2	0.0
16FGAC297	547948.88	9227101.00	46.03	0	90	12	0	4.5	4.5	1.3	11.9	7.1	0.0
16FGAC298	547899.00	9227100.00	46.67	0	90	12	0	4.5	4.5	1.6	16.6	5.8	0.0
16FGAC299	547850.38	9227102.00	45.25	0	90	12	0	7.5	7.5	4.2	26.4	5.5	0.1
16FGAC300	547796.69	9227092.00	45.51	0	90	12	0	7.5	7.5	4.1	26.1	6.4	0.5
16FGAC300	547796.69	9227092.00	39.51	0	90	12	9	10.5	1.5	2.6	41.2	3.4	0.0
16FGAC301	547800.69	9226982.00	45.86	0	90	12	0	7.5	7.5	2.3	31.9	5.9	0.2
16FGAC302	547851.75	9226998.00	45.93	0	90	12	0	7.5	7.5	3.9	24.5	5.3	0.2
16FGAC302	547851.75	9226998.00	39.93	0	90	12	9	10.5	1.5	1.6	32.4	7.2	0.1
16FGAC303	547901.38	9226995.00	46.77	0	90	12	0	6	6	3.7	23.4	8.5	0.4
16FGAC303	547901.38	9226995.00	40.02	0	90	12	9	10.5	1.5	1.1	24.6	11.6	0.1
16FGAC304	547950.63	9226998.00	47.07	0	90	12	0	4.5	4.5	1.6	17.3	6.2	0.0
16FGAC305	548001.81	9227002.00	45.74	0	90	12	0	6	6	1.4	19.7	8.5	0.2
16FGAC306	548049.81	9227000.00	43.89	0	90	12	0	7.5	7.5	4.7	22.3	7.4	0.4
16FGAC306	548049.81	9227000.00	36.39	0	90	12	10.5	12	1.5	1.1	38.1	1.4	0.0
16FGAC307	548101.75	9226998.00	43.02	0	90	12	0	6	6	4.4	17.8	5.8	0.2
16FGAC308	548154.00	9227002.00	40.75	0	90	12	1.5	3	1.5	1.0	16.1	14.7	1.5
16FGAC308	548154.00	9227002.00	32.50	0	90	12	9	12	3	1.1	19.0	10.7	0.3
16FGAC309	548150.25	9226901.00	37.42	0	90	12	0	6	6	2.5	17.7	8.1	0.8
16FGAC309	548150.25	9226901.00	29.17	0	90	12	10.5	12	1.5	1.1	33.4	2.8	0.0
16FGAC310	548099.94	9226900.00	42.10	0	90	12	0	4.5	4.5	5.2	12.4	11.1	1.9
16FGAC311	548050.88	9226903.00	43.81	0	90	12	0	7.5	7.5	3.4	24.9	13.2	1.0
16FGAC312	547951.50	9226902.00	46.78	0	90	12	0	6	6	3.0	20.5	9.7	1.2
16FGAC313	547898.19	9226899.00	45.50	0	90	12	0	9	9	2.5	25.4	7.9	0.2
16FGAC314	547849.94	9226898.00	46.25	0	90	12	0	7.5	7.5	2.2	24.6	7.0	0.1

16FGAC315	547800.13	9226901.00	46.25	0	90	12	0	7.5	7.5	1.6	28.4	6.7	0.0
16FGAC316	547949.19	9226799.00	46.78	0	90	12	0	6	6	2.4	27.1	5.0	0.0
16FGAC317	547997.94	9226802.00	45.61	0	90	12	0	6	6	3.1	22.8	7.9	0.3
16FGAC317	547997.94	9226802.00	37.36	0	90	12	10.5	12	1.5	1.4	44.1	2.1	0.0
16FGAC318	548049.50	9226798.00	38.51	0	90	12	0	12	12	3.9	24.9	9.8	0.3
16FGAC319	548099.44	9226800.00	36.45	0	90	12	0	10.5	10.5	5.5	20.3	6.4	0.1
16FGAC320	548143.19	9226700.00	36.31	0	90	12	0	9	9	10.1	21.8	10.1	1.0
16FGAC321	548048.94	9226698.00	38.04	0	90	12	0	9	9	7.2	18.3	8.0	0.3
16FGAC322	547899.69	9226601.00	46.55	0	90	12	0	4.5	4.5	1.3	24.5	6.8	0.2
16FGAC323	547948.31	9226602.00	44.58	0	90	12	0	3	3	1.2	14.9	9.8	0.0
16FGAC324	547994.38	9226603.00	40.23	0	90	12	0	6	6	5.0	14.3	3.9	0.0
16FGAC325	548049.50	9226597.00	37.92	0	90	12	0	9	9	4.1	25.2	5.5	0.2
16FGAC326	548102.75	9226602.00	38.01	0	90	12	0	9	9	14.2	23.1	7.3	0.2
16FGAC327	548150.63	9226601.00	35.35	0	90	12	0	12	12	7.7	27.4	9.5	0.4
16FGAC328	548150.13	9226500.00	35.80	0	90	12	0	12	12	8.6	18.5	10.3	0.7
16FGAC329	548046.44	9226503.00	38.23	0	90	12	0	9	9	4.2	23.7	3.5	0.0
16FGAC330	547949.25	9226502.00	40.64	0	90	12	0	4.5	4.5	1.4	12.0	4.1	0.0
16FGAC331	547851.13	9226501.00	48.41	0	90	12	0	1.5	1.5	1.0	14.1	6.6	0.0
16FGAC332	547899.25	9226400.00	40.49	0	90	12	1.5	3	1.5	1.1	21.2	5.8	0.0
16FGAC333	547950.06	9226400.00	39.75	0	90	12	0	4.5	4.5	2.3	20.0	5.2	0.0
16FGAC333	547950.06	9226400.00	30.75	0	90	12	10.5	12	1.5	1.1	19.4	0.3	0.0
16FGAC334	547999.75	9226401.00	38.26	0	90	12	0	7.5	7.5	2.6	20.5	5.4	0.1
16FGAC334	547999.75	9226401.00	31.51	0	90	12	9	12	3	1.5	33.8	9.2	0.0
16FGAC335	548050.56	9226401.00	37.50	0	90	12	0	9	9	6.8	20.0	8.5	0.6
16FGAC336	548098.81	9226400.00	35.78	0	90	12	0	12	12	5.5	24.0	9.3	0.5
16FGAC337	548150.63	9226400.00	35.45	0	90	12	0	12	12	4.4	21.8	7.9	0.6
16FGAC338	548198.44	9226402.00	37.50	0	90	12	0	7.5	7.5	9.5	17.4	8.0	1.0
16FGAC339	548248.25	9226403.00	38.00	0	90	12	0	6	6	8.9	18.2	6.8	0.3
16FGAC340	548300.00	9226402.00	37.25	0	90	12	0	7.5	7.5	2.7	26.7	6.5	0.2
16FGAC340	548300.00	9226402.00	29.75	0	90	12	10.5	12	1.5	1.4	54.5	0.5	0.0
16FGAC342	548352.06	9226801.00	29.50	0	90	15	6	15	9	2.3	18.5	12.0	0.9
16FGAC343	548299.00	9226801.00	34.75	0	90	15	4.5	6	1.5	1.3	26.1	10.4	0.8
16FGAC344	548248.44	9226799.00	31.75	0	90	12	7.5	9	1.5	1.1	29.8	9.1	0.7
16FGAC344	548248.44	9226799.00	28.75	0	90	12	10.5	12	1.5	1.4	18.7	7.4	0.0
16FGAC345	548201.06	9226701.00	35.50	0	90	12	0	9	9	3.0	25.0	5.7	0.3
16FGAC346	548250.13	9226697.00	38.50	0	90	12	0	3	3	1.4	21.5	3.1	0.0
16FGAC346	548250.13	9226697.00	34.00	0	90	12	4.5	7.5	3	1.6	26.3	5.5	0.3
16FGAC347	548303.31	9226699.00	29.50	0	90	15	7.5	13.5	6	2.1	21.7	6.9	0.1
16FGAC349	548351.81	9226304.00	39.50	0	90	12	0	3	3	1.4	6.0	8.2	0.0
16FGAC350	548249.94	9226300.00	36.80	0	90	12	0	9	9	6.7	26.4	7.5	0.2
16FGAC351	548051.38	9226300.00	36.00	0	90	12	0	12	12	6.5	20.4	8.4	0.4
16FGAC352	547948.81	9226300.00	39.00	0	90	12	0	6	6	2.2	21.1	6.2	0.1
16FGAC352	547948.81	9226300.00	30.75	0	90	12	10.5	12	1.5	1.0	40.9	18.7	0.0

16FGAC353	547899.44	9226200.00	40.50	0	90	12	0	3	3	1.3	3.7	7.9	0.0
16FGAC354	547952.75	9226208.00	39.75	0	90	12	0	4.5	4.5	4.4	8.5	3.6	0.0
16FGAC354	547952.75	9226208.00	34.50	0	90	12	6	9	3	1.7	34.1	13.3	0.0
16FGAC355	547999.88	9226199.00	36.00	0	90	12	0	12	12	5.4	20.5	7.8	0.2
16FGAC356	548050.31	9226200.00	36.00	0	90	12	0	12	12	7.5	24.1	6.7	0.3
16FGAC357	548100.31	9226200.00	36.00	0	90	15	0	12	12	8.5	16.9	9.0	0.4
16FGAC357	548100.31	9226200.00	27.75	0	90	15	13.5	15	1.5	1.3	24.5	5.5	0.1
16FGAC358	548149.94	9226199.00	34.50	0	90	15	0	15	15	10.4	16.6	8.4	0.3
16FGAC359	548199.50	9226200.00	37.50	0	90	15	0	9	9	6.5	26.0	8.1	0.5
16FGAC359	548199.50	9226200.00	27.75	0	90	15	13.5	15	1.5	1.1	27.9	3.5	0.0
16FGAC360	548250.94	9226199.00	36.00	0	90	12	0	12	12	3.3	16.9	7.6	0.1
16FGAC361	548299.56	9226199.00	37.96	0	90	12	0	7.5	7.5	2.5	19.9	5.7	0.2
16FGAC362	548350.31	9226199.00	40.15	0	90	12	0	3	3	1.2	9.1	3.0	0.0
16FGAC363	548299.19	9226099.00	40.50	0	90	12	0	3	3	1.4	7.7	3.8	0.0
16FGAC364	548252.38	9226099.00	38.25	0	90	12	0	7.5	7.5	1.9	15.0	2.5	0.1
16FGAC365	548149.25	9226098.00	36.75	0	90	12	0	10.5	10.5	9.3	32.0	6.0	0.4
16FGAC366	548051.75	9226102.00	36.75	0	90	12	0	10.5	10.5	4.9	15.1	6.5	0.3
16FGAC367	547850.81	9226102.00	39.75	0	90	12	1.5	3	1.5	1.1	12.0	5.6	0.0
16FGAC367	547850.81	9226102.00	36.75	0	90	12	4.5	6	1.5	1.0	26.0	4.8	0.1
16FGAC367	547850.81	9226102.00	31.50	0	90	12	9	12	3	1.2	32.9	9.7	0.0
16FGAC368	547750.50	9226100.00	40.43	0	90	12	0	4.5	4.5	2.0	15.5	3.7	0.0
16FGAC369	547700.50	9226100.00	40.56	0	90	12	0	7.5	7.5	2.9	13.1	5.6	0.2
16FGAC370	547651.13	9226100.00	45.16	0	90	12	0	4.5	4.5	2.5	13.3	7.9	0.1
16FGAC372	547896.50	9225998.00	39.00	0	90	12	0	6	6	2.3	21.1	4.6	0.2
16FGAC373	547850.13	9225903.00	39.00	0	90	12	0	6	6	2.3	9.3	4.9	0.0
16FGAC374	547748.25	9225904.00	39.75	0	90	12	0	4.5	4.5	1.8	16.6	9.6	0.0
16FGAC376	548199.88	9226000.00	36.95	0	90	12	1.5	9	7.5	2.0	17.2	2.1	0.0
16FGAC377	548145.06	9225997.00	34.50	0	90	15	0	15	15	3.4	19.2	4.5	0.1
16FGAC378	548097.19	9225983.00	36.75	0	90	12	0	10.5	10.5	3.3	18.8	6.8	0.2
16FGAC379	548047.31	9225999.00	39.75	0	90	12	0	4.5	4.5	5.0	10.5	6.0	0.0
16FGAC379	548047.31	9225999.00	34.50	0	90	12	6	9	3	1.8	23.2	4.4	0.1
16FGAC381	548150.69	9225899.00	39.25	0	90	15	0	7.5	7.5	1.2	8.3	2.5	0.1
16FGAC382	548105.13	9225902.00	35.16	0	90	15	0	15	15	2.6	16.3	6.7	0.2
16FGAC383	548052.44	9225899.00	39.75	0	90	15	0	4.5	4.5	5.1	10.0	4.4	0.0
16FGAC383	548052.44	9225899.00	34.50	0	90	15	6	9	3	1.9	24.4	4.6	0.2
16FGAC384	548148.06	9225805.00	35.25	0	90	12	7.5	9	1.5	1.2	15.3	5.9	0.3
16FGAC385	548099.06	9225799.00	39.95	0	90	12	1.5	4.5	3	1.0	8.3	2.7	0.0
16FGAC385	548099.06	9225799.00	35.45	0	90	12	6	9	3	1.6	16.7	5.3	0.1
16FGAC386	548049.06	9225800.00	36.71	0	90	12	0	12	12	1.7	14.3	6.3	0.1
16FGAC387	548010.63	9225796.00	37.64	0	90	12	0	9	9	3.0	15.5	5.1	0.2
16FGAC388	548054.38	9225701.00	34.17	0	90	12	7.5	10.5	3	1.2	17.5	6.8	0.1
16FGAC389	547955.25	9225701.00	37.40	0	90	12	0	10.5	10.5	3.4	16.3	5.3	0.2
16FGAC391	547899.25	9225601.00	39.58	0	90	12	0	6	6	2.4	7.0	5.9	0.0

16FGAC391	547899.25	9225601.00	31.33	0	90	12	10.5	12	1.5	1.4	24.6	8.3	0.3
16FGAC392	547851.94	9225601.00	36.00	0	90	12	0	12	12	2.0	15.7	5.8	0.1
16FGAC393	547795.69	9225599.00	39.75	0	90	12	0	4.5	4.5	2.2	12.2	4.3	0.4
16FGAC394	547750.50	9225600.00	39.00	0	90	12	0	6	6	3.2	18.8	3.2	0.0
16FGAC394	547750.50	9225600.00	30.75	0	90	12	10.5	12	1.5	1.1	30.2	2.6	0.0
16FGAC395	547701.94	9225601.00	40.45	0	90	12	0	4.5	4.5	1.6	13.3	6.8	0.1
16FGAC396	547650.38	9225600.00	41.25	0	90	12	0	6	6	2.8	11.3	8.4	0.6
16FGAC397	547601.63	9225599.00	41.08	0	90	12	1.5	9	7.5	1.6	17.6	8.7	0.2
16FGAC398	547550.56	9225601.00	38.83	0	90	12	7.5	12	4.5	1.8	25.0	8.4	0.1
16FGAC399	547549.56	9225700.00	46.45	0	90	12	0	4.5	4.5	1.3	22.0	8.4	0.2
16FGAC400	547647.38	9225699.00	39.38	0	90	12	1.5	4.5	3	1.5	22.6	8.0	0.6
16FGAC401	547600.19	9225500.00	41.37	0	90	12	3	7.5	4.5	1.4	24.0	5.4	0.0
16FGAC402	547650.31	9225498.00	40.72	0	90	12	1.5	6	4.5	1.5	12.9	9.9	0.1
16FGAC403	547749.94	9225501.00	39.83	0	90	12	0	4.5	4.5	1.9	10.3	1.7	0.0
16FGAC405	547651.00	9225400.00	40.54	0	90	12	0	4.5	4.5	1.8	11.2	7.8	0.1
16FGAC406	547701.00	9225399.00	39.78	0	90	12	0	4.5	4.5	1.7	15.3	1.5	0.0
16FGAC407	547750.75	9225396.00	39.75	0	90	12	0	4.5	4.5	2.3	9.5	1.3	0.0
16FGAC408	547799.75	9225399.00	39.00	0	90	12	0	6	6	1.6	14.1	1.5	0.0
16FGAC409	547850.75	9225400.00	35.40	0	90	12	6	7.5	1.5	1.5	3.8	2.0	0.0
16FGAC410	547897.94	9225399.00	38.95	0	90	12	3	4.5	1.5	1.0	10.7	1.9	0.0
16FGAC410	547897.94	9225399.00	32.95	0	90	12	9	10.5	1.5	1.2	22.4	10.5	0.6
16FGAC411	547850.94	9225501.00	38.42	0	90	12	3	4.5	1.5	1.1	14.7	1.6	0.0
16FGAC412	547904.19	9225502.00	37.65	0	90	12	4.5	6	1.5	1.1	7.3	2.5	0.0
16FGAC413	547797.94	9225301.00	30.78	0	90	12	10.5	12	1.5	1.3	19.4	5.7	0.0
16FGAC415	547703.94	9225302.00	39.75	0	90	12	0	4.5	4.5	2.4	8.9	1.2	0.0
16FGAC416	547650.56	9225323.00	39.00	0	90	12	0	6	6	2.4	16.1	2.0	0.0
16FGAC416	547650.56	9225323.00	30.75	0	90	12	10.5	12	1.5	1.0	35.0	3.8	0.0
16FGAC419	547498.31	9225303.00	43.15	0	90	12	0	9	9	1.7	17.2	7.1	0.1
16FGAC421	547401.19	9225198.00	50.56	0	90	12	1.5	7.5	6	1.4	26.5	6.7	0.4
16FGAC422	547449.31	9225210.00	46.04	0	90	12	0	7.5	7.5	2.5	24.5	6.3	0.3
16FGAC423	547499.13	9225198.00	41.36	0	90	12	0	9	9	4.3	14.4	5.8	0.1
16FGAC424	547548.50	9225198.00	41.20	0	90	12	0	4.5	4.5	1.7	3.6	7.4	0.0
16FGAC425	547596.94	9225179.00	38.11	0	90	12	0	7.5	7.5	2.5	12.8	7.4	0.4
16FGAC425	547596.94	9225179.00	30.61	0	90	12	10.5	12	1.5	1.5	28.5	2.2	0.0
16FGAC426	547650.38	9225199.00	39.30	0	90	12	0	4.5	4.5	2.3	8.1	1.8	0.0
16FGAC426	547650.38	9225199.00	30.30	0	90	12	10.5	12	1.5	1.1	39.7	3.8	0.0
16FGAC428	547598.63	9225099.00	37.24	0	90	12	0	9	9	1.7	14.4	6.7	0.2
16FGAC429	547552.31	9225100.00	40.35	0	90	12	0	4.5	4.5	3.1	9.8	3.0	0.0
16FGAC429	547552.31	9225100.00	35.85	0	90	12	6	7.5	1.5	1.3	27.0	2.4	0.0
16FGAC430	547502.13	9225100.00	40.75	0	90	12	0	7.5	7.5	1.9	11.7	8.4	0.3
16FGAC431	547450.44	9225100.00	43.65	0	90	12	0	7.5	7.5	2.3	8.8	6.3	0.0
16FGAC432	547849.00	9226204.00	17.25	0	90	57	19.5	30	10.5	1.9	18.2	16.5	0.3
16FGAC432	547849.00	9226204.00	-4.50	0	90	57	42	51	9	2.5	23.4	3.6	0.0

16FGAC432	547849.00	9226204.00	-13.50	0	90	57	54	57	3	1.6	11.6	17.4	0.1
16FGAC1110	547898.00	9226789.00	47.00	0	90	12	0	6	6	2.2	22.4	4.2	0.1
16FGAC1111	547851.00	9226805.00	47.00	0	90	12	0	6	6	1.5	22.9	3.9	0.0
16FGAC1112	547800.00	9226801.00	47.00	0	90	12	0	6	6	1.7	24.0	6.6	0.7
16FGAC1113	547745.00	9227002.00	45.89	0	90	12	0	7.5	7.5	1.8	22.9	6.0	0.5
16FGAC1114	547703.00	9227005.00	46.00	0	90	12	0	6	6	2.0	19.7	4.6	0.0
16FGAC1114	547703.00	9227005.00	37.75	0	90	12	10.5	12	1.5	1.2	22.5	4.1	0.0
16FGAC1115	547653.00	9227009.00	46.00	0	90	12	0	6	6	2.2	22.4	7.2	0.2
16FGAC1116	547595.00	9227102.00	46.75	0	90	12	0	4.5	4.5	2.5	16.5	4.6	0.0
16FGAC1117	547647.00	9227089.00	46.00	0	90	12	0	6	6	3.7	21.7	5.7	0.1
16FGAC1118	547700.00	9227091.00	45.92	0	90	12	0	6	6	1.8	21.3	5.3	0.1
16FGAC1119	547753.00	9227107.00	46.62	0	90	12	0	4.5	4.5	3.5	21.2	4.3	0.1
16FGAC1119	547753.00	9227107.00	39.12	0	90	12	9	10.5	1.5	1.1	32.7	3.6	0.3
16FGAC1120	548099.00	9227100.00	44.62	0	90	12	0	3	3	1.2	12.1	4.4	0.0
16FGAC1120	548099.00	9227100.00	35.62	0	90	12	9	12	3	1.1	27.9	10.0	0.2
16FGAC1121	548149.00	9227104.00	36.86	0	90	12	6	9	3	1.7	21.2	14.9	0.2
16FGAC1122	548148.00	9227206.00	36.35	0	90	12	6	9	3	1.2	21.8	10.5	0.1
16FGAC1122	548148.00	9227206.00	32.60	0	90	12	10.5	12	1.5	1.3	22.4	3.5	0.2
16FGAC1124	548047.00	9227202.00	44.81	0	90	12	0	3	3	1.5	8.4	4.3	0.0
16FGAC1125	547989.00	9227207.00	44.59	0	90	12	0	4.5	4.5	1.7	12.8	7.7	0.3
16FGAC1126	547937.00	9227195.00	45.78	0	90	12	0	3	3	1.2	13.4	7.4	0.0
16FGAC1127	547900.00	9227197.00	45.12	0	90	12	0	4.5	4.5	1.2	19.3	7.1	0.0
16FGAC1128	547848.00	9227197.00	44.92	0	90	12	0	4.5	4.5	1.7	21.1	6.6	0.1
16FGAC1129	547803.00	9227201.00	44.16	0	90	12	0	7.5	7.5	3.5	22.1	4.5	0.1
16FGAC1129	547803.00	9227201.00	36.66	0	90	12	10.5	12	1.5	1.5	39.2	6.5	0.1
16FGAC1130	547751.00	9227203.00	44.95	0	90	12	0	7.5	7.5	4.0	24.7	4.4	0.2
16FGAC1131	547699.00	9227207.00	46.00	0	90	30	0	6	6	2.5	27.9	3.5	0.0
16FGAC1131	547699.00	9227207.00	31.75	0	90	30	16.5	18	1.5	1.0	35.0	2.3	0.0
16FGAC1131	547699.00	9227207.00	25.75	0	90	30	22.5	24	1.5	1.4	25.3	10.3	1.0
16FGAC1131	547699.00	9227207.00	20.50	0	90	30	27	30	3	1.1	27.9	3.2	0.0
16FGAC1132	547650.00	9227205.00	46.75	0	90	12	0	4.5	4.5	2.6	21.2	3.3	0.0
16FGAC1133	547603.00	9227205.00	46.00	0	90	12	0	6	6	3.0	22.6	4.8	0.0
16FGAC1134	547549.00	9227201.00	47.50	0	90	12	0	3	3	1.2	9.8	6.8	0.0
16FGAC1135	547501.00	9227202.00	48.25	0	90	12	0	1.5	1.5	1.1	5.6	3.3	0.0
16FGAC1135	547501.00	9227202.00	42.25	0	90	12	6	7.5	1.5	1.1	28.6	7.2	0.2
16FGAC1136	547404.00	9227404.00	48.25	0	90	12	0	1.5	1.5	1.1	5.7	2.9	0.0
16FGAC1136	547404.00	9227404.00	45.25	0	90	12	3	4.5	1.5	1.5	17.7	2.4	0.0
16FGAC1137	547452.00	9227401.00	48.25	0	90	12	0	1.5	1.5	1.1	7.1	2.7	0.0
16FGAC1137	547452.00	9227401.00	45.25	0	90	12	3	4.5	1.5	1.1	25.0	3.9	0.0
16FGAC1138	547497.00	9227400.00	45.25	0	90	12	0	7.5	7.5	1.9	20.8	5.2	0.0
16FGAC1139	547548.00	9227402.00	46.75	0	90	12	0	4.5	4.5	3.0	18.3	4.0	0.0
16FGAC1139	547548.00	9227402.00	37.75	0	90	12	10.5	12	1.5	1.0	23.6	4.0	0.0
16FGAC1140	547600.00	9227398.00	46.75	0	90	12	0	4.5	4.5	2.1	15.9	3.7	0.0

16FGAC1141	547653.00	9227402.00	45.74	0	90	12	0	6	6	3.1	22.0	5.0	0.1
16FGAC1142	547697.00	9227401.00	45.00	0	90	30	0	6	6	4.0	26.5	5.9	0.3
16FGAC1142	547697.00	9227401.00	29.25	0	90	30	16.5	21	4.5	1.2	42.3	4.9	0.2
16FGAC1142	547697.00	9227401.00	23.25	0	90	30	22.5	27	4.5	1.6	28.3	10.0	0.3
16FGAC1143	547751.00	9227398.00	45.55	0	90	12	0	4.5	4.5	2.0	19.6	4.7	0.0
16FGAC1144	547798.00	9227400.00	45.26	0	90	12	0	4.5	4.5	1.3	14.9	6.8	0.0
16FGAC1145	547847.00	9227400.00	45.60	0	90	12	1.5	3	1.5	1.0	14.4	4.2	0.0
16FGAC1146	547897.00	9227405.00	44.33	0	90	12	1.5	3	1.5	1.1	19.6	5.6	0.0
16FGAC1147	547946.00	9227370.00	44.51	0	90	12	0	3	3	1.9	11.9	3.9	0.0
16FGAC1150	547999.00	9227608.00	37.75	0	90	12	7.5	9	1.5	1.1	19.2	9.3	0.2
16FGAC1150	547999.00	9227608.00	34.75	0	90	12	10.5	12	1.5	1.2	20.5	11.3	0.3
16FGAC1153	547854.00	9227606.00	44.50	0	90	12	0	3	3	1.9	16.6	7.8	0.6
16FGAC1154	547803.00	9227604.00	35.37	0	90	12	10.5	12	1.5	1.1	44.3	4.4	0.3
16FGAC1156	547702.00	9227604.00	45.66	0	90	30	0	4.5	4.5	1.5	17.0	4.0	0.0
16FGAC1156	547702.00	9227604.00	20.16	0	90	30	27	28.5	1.5	1.2	31.9	5.6	0.0
16FGAC1157	547657.00	9227593.00	45.77	0	90	12	0	4.5	4.5	1.3	12.9	6.3	0.0
16FGAC1157	547657.00	9227593.00	36.77	0	90	12	10.5	12	1.5	1.1	26.9	7.5	0.2
16FGAC1158	547600.00	9227603.00	46.32	0	90	12	0	4.5	4.5	2.9	16.4	5.5	0.0
16FGAC1159	547550.00	9227603.00	45.63	0	90	12	0	6	6	2.1	18.3	2.6	0.0
16FGAC1160	547502.00	9227603.00	45.77	0	90	12	0	6	6	2.4	18.7	4.8	0.1
16FGAC1161	547445.00	9227607.00	46.75	0	90	12	0	4.5	4.5	2.9	14.6	4.8	0.0
16FGAC1162	547402.00	9227610.00	47.83	0	90	12	0	1.5	1.5	1.3	6.2	2.3	0.0
16FGAC1162	547402.00	9227610.00	44.83	0	90	12	3	4.5	1.5	1.3	24.4	4.1	0.0
16FGAC1164	547400.00	9227800.00	45.00	0	90	12	0	6	6	1.7	19.0	6.1	0.0
16FGAC1165	547450.00	9227802.00	45.93	0	90	12	0	4.5	4.5	2.2	16.4	4.0	0.0
16FGAC1166	547502.00	9227798.00	45.00	0	90	12	0	6	6	1.7	17.5	6.0	0.0
16FGAC1167	547556.00	9227800.00	36.52	0	90	12	10.5	12	1.5	1.3	39.9	3.8	0.2
16FGAC1169	547644.00	9227801.00	36.64	0	90	12	10.5	12	1.5	1.1	20.8	3.4	0.0
16FGAC1170	547687.00	9227796.00	19.65	0	90	30	27	28.5	1.5	1.1	21.6	18.6	0.8
16FGAC1171	547741.00	9227800.00	45.24	0	90	12	0	3	3	1.4	18.4	6.1	0.0
16FGAC1172	547797.00	9227803.00	43.74	0	90	12	0	4.5	4.5	2.5	21.4	3.7	0.0
16FGAC1173	547850.00	9227802.00	44.17	0	90	12	0	3	3	1.2	17.3	9.1	0.5
16FGAC1175	547948.00	9227800.00	39.25	0	90	12	6	7.5	1.5	1.0	27.3	10.7	0.8
16FGAC1179	547805.00	9227994.00	43.75	0	90	12	0	4.5	4.5	2.4	21.2	5.9	0.0
16FGAC1180	547752.00	9227999.00	44.32	0	90	12	0	4.5	4.5	6.4	24.8	2.9	0.1
16FGAC1181	547709.00	9228003.00	44.75	0	90	30	0	4.5	4.5	3.4	31.5	2.6	0.0
16FGAC1181	547709.00	9228003.00	36.50	0	90	30	6	15	9	1.3	25.7	7.0	0.2
16FGAC1181	547709.00	9228003.00	26.75	0	90	30	19.5	21	1.5	1.4	19.4	7.1	0.2
16FGAC1182	547647.00	9227999.00	46.40	0	90	12	0	1.5	1.5	1.1	16.1	2.9	0.0
16FGAC1187	547402.00	9227999.00	45.00	0	90	12	0	6	6	2.0	17.2	6.3	0.2
16FGAC1188	547351.00	9227997.00	45.00	0	90	12	0	6	6	2.5	22.5	3.8	0.0
16FGAC1189	547301.00	9228000.00	46.25	0	90	12	0	4.5	4.5	1.6	11.7	3.6	0.0
16FGAC1190	547300.00	9228202.00	45.52	0	90	12	0	4.5	4.5	1.9	16.5	7.0	0.1

16FGAC1191	547350.00	9228200.00	45.75	0	90	12	0	4.5	4.5	1.3	15.0	7.3	0.0
16FGAC1192	547400.00	9228201.00	45.38	0	90	12	1.5	3	1.5	1.0	15.2	6.1	0.0
16FGAC1196	547607.00	9228217.00	46.12	0	90	12	0	3	3	2.0	6.9	3.7	0.0
16FGAC1196	547607.00	9228217.00	40.87	0	90	12	6	7.5	1.5	1.2	45.4	1.1	0.0
16FGAC1196	547607.00	9228217.00	36.37	0	90	12	10.5	12	1.5	1.0	36.8	3.6	0.0
16FGAC1197	547648.00	9228198.00	44.78	0	90	12	0	4.5	4.5	3.2	28.0	3.4	0.0
16FGAC1198	547708.00	9228201.00	44.33	0	90	30	0	4.5	4.5	5.6	27.6	7.7	0.3
16FGAC1198	547708.00	9228201.00	31.58	0	90	30	13.5	16.5	3	1.3	33.7	4.2	0.1
16FGAC1198	547708.00	9228201.00	18.08	0	90	30	27	30	3	1.1	19.4	2.0	0.0
16FGAC1199	547749.00	9228196.00	44.00	0	90	12	0	4.5	4.5	4.6	20.1	2.5	0.0
16FGAC1200	547792.00	9228200.00	44.40	0	90	12	0	3	3	1.3	9.9	2.6	0.0
16FGAC1203	547949.00	9228198.00	40.11	0	90	12	4.5	6	1.5	1.2	31.4	6.6	0.1
16FGAC1203	547949.00	9228198.00	34.86	0	90	12	9	12	3	1.0	30.3	12.7	0.8
16FGAC1204	547850.00	9228402.00	44.25	0	90	12	0	1.5	1.5	1.5	32.4	1.7	0.0
16FGAC1204	547850.00	9228402.00	39.75	0	90	12	3	7.5	4.5	1.2	27.3	8.3	0.4
16FGAC1206	547750.00	9228397.00	45.25	0	90	12	0	1.5	1.5	1.1	16.3	2.8	0.0
16FGAC1207	547704.00	9228398.00	43.82	0	90	30	0	4.5	4.5	3.0	21.4	3.8	0.1
16FGAC1207	547704.00	9228398.00	36.32	0	90	30	9	10.5	1.5	1.1	31.4	3.6	0.0
16FGAC1207	547704.00	9228398.00	24.32	0	90	30	16.5	27	10.5	1.2	25.8	7.2	0.2
16FGAC1207	547704.00	9228398.00	16.82	0	90	30	28.5	30	1.5	1.2	15.8	25.9	1.8
16FGAC1208	547652.00	9228397.00	43.75	0	90	12	0	4.5	4.5	6.1	27.4	4.4	0.0
16FGAC1208	547652.00	9228397.00	37.00	0	90	12	6	12	6	1.6	34.1	3.5	0.2
16FGAC1209	547602.00	9228399.00	44.29	0	90	12	0	4.5	4.5	4.7	29.3	4.2	0.0
16FGAC1210	547554.00	9228400.00	44.96	0	90	12	0	4.5	4.5	1.6	14.6	4.1	0.0
16FGAC1213	547399.00	9228404.00	37.92	0	90	12	9	10.5	1.5	1.1	24.1	5.3	0.3
16FGAC1216	547500.00	9228603.00	45.05	0	90	30	0	3	3	1.8	10.7	3.2	0.0
16FGAC1216	547500.00	9228603.00	17.30	0	90	30	28.5	30	1.5	1.1	37.1	2.6	0.7
16FGAC1217	547549.00	9228602.00	43.67	0	90	12	0	4.5	4.5	4.7	18.2	6.4	0.2
16FGAC1218	547607.00	9228606.00	43.63	0	90	12	0	4.5	4.5	1.8	16.8	9.2	0.2
16FGAC1219	547648.00	9228603.00	43.69	0	90	12	0	3	3	1.5	13.9	2.7	0.0
16FGAC1220	547701.00	9228612.00	38.25	0	90	12	6	7.5	1.5	1.1	26.3	9.0	0.4
16FGAC1221	547747.00	9228603.00	41.25	0	90	12	3	4.5	1.5	1.0	30.7	3.0	0.0
16FGAC1221	547747.00	9228603.00	35.25	0	90	12	9	10.5	1.5	1.3	28.2	3.6	0.0
16FGAC1222	547797.00	9228607.00	39.75	0	90	12	4.5	6	1.5	1.0	31.3	3.4	0.2
16FGAC1223	547702.00	9228801.00	38.25	0	90	12	6	7.5	1.5	1.0	29.0	6.0	0.0
16FGAC1225	547599.00	9228805.00	42.75	0	90	12	0	4.5	4.5	1.2	15.9	4.2	0.0
16FGAC1226	547550.00	9228804.00	43.61	0	90	12	0	3	3	2.2	18.9	5.0	0.0
16FGAC1227	547501.00	9228806.00	42.81	0	90	30	0	4.5	4.5	3.6	17.1	8.6	0.3
16FGAC1227	547501.00	9228806.00	38.31	0	90	30	6	7.5	1.5	1.0	53.8	1.9	0.0
16FGAC1227	547501.00	9228806.00	16.56	0	90	30	27	30	3	1.4	20.6	2.5	0.0
16FGAC1228	547451.00	9228800.00	43.36	0	90	12	0	4.5	4.5	1.5	13.0	5.7	0.0
16FGAC1228	547451.00	9228800.00	35.86	0	90	12	9	10.5	1.5	1.4	25.2	11.8	1.6
16FGAC1234	547399.00	9229001.00	42.62	0	90	12	0	4.5	4.5	2.5	18.8	6.8	0.0

16FGAC1234	547399.00	9229001.00	38.12	0	90	12	6	7.5	1.5	1.2	36.6	2.1	0.0
16FGAC1235	547449.00	9229002.00	41.75	0	90	30	0	4.5	4.5	3.9	21.8	9.0	0.3
16FGAC1236	547500.00	9229000.00	41.75	0	90	12	0	4.5	4.5	1.7	14.7	5.3	0.1
16FGAC1241	547401.00	9229203.00	40.75	0	90	12	0	4.5	4.5	2.5	19.1	9.0	0.4
16FGAC1242	547353.00	9229197.00	40.00	0	90	12	0	6	6	2.1	19.4	7.5	0.3
16FGAC1245	547250.00	9229401.00	40.54	0	90	12	1.5	3	1.5	1.2	19.0	4.3	0.0

Appendix 3. Modal mineral assemblage analysis data for composite samples

Resource Area	Composite Number	Ilmenite	Zircon	Rutile	Leucoxene	Nonmag others	Mag others	Monazite	VHM	TRASH	THM Domain
Fungoni	Z2-001	40.4	13.5	3.3	1.0	39.3	0.9	1.5	58.2	41.8	High Grade Domain 2
Fungoni	Z2-002	23.8	10.2	2.7	1.2	59.4	1.9	0.7	38.0	62.0	High Grade Domain 2
Fungoni	Z2-003	36.1	13.7	3.0	1.2	42.8	1.9	1.3	54.0	46.0	High Grade Domain 2
Fungoni	Z2-004	36.5	12.7	4.6	1.8	39.0	4.8	0.6	55.6	44.4	High Grade Domain 2
Fungoni	Z2-005	44.8	18.8	4.3	1.7	28.3	0.7	1.5	69.6	30.4	High Grade Domain 2
Fungoni	Z2-006	46.3	22.3	4.3	0.8	23.0	1.5	1.8	73.7	26.3	High Grade Domain 2
Fungoni	Z2-007	43.8	20.8	4.9	0.8	25.5	2.0	2.1	70.3	29.7	High Grade Domain 2
Fungoni	Z2-008	46.2	22.4	4.2	1.2	23.3	0.9	1.7	74.1	25.9	High Grade Domain 2
Fungoni	Z2-009	47.7	14.2	5.2	0.7	30.6	0.7	0.8	67.9	32.1	High Grade Domain 2
Fungoni	Z2-010	46.9	13.4	4.1	0.4	33.3	1.0	0.9	64.8	35.2	High Grade Domain 2
Fungoni NW	Z2-011	37.5	10.4	4.6	1.1	38.8	6.9	0.6	53.6	46.4	High Grade Domain 2
Fungoni NW	Z2-012	34.2	10.1	4.6	1.6	40.9	8.0	0.5	50.5	49.5	High Grade Domain 2
Fungoni NW	Z2-013	38.3	24.2	5.4	2.1	22.6	4.5	2.8	70.1	29.9	High Grade Domain 2
Fungoni NW	Z2-014	33.0	16.1	4.8	2.1	35.1	7.5	1.4	55.9	44.1	High Grade Domain 2
Fungoni	Z4-001	37.9	11.6	3.9	0.7	43.8	1.5	0.6	54.1	45.9	Mod Grade Domain 4
Fungoni	Z4-002	34.4	9.0	2.8	0.6	50.2	2.0	0.9	46.9	53.1	Mod Grade Domain 4
Fungoni	Z5-001	35.2	8.0	4.1	0.7	44.6	6.4	1.0	47.9	52.1	Low Grade Domain 5
Fungoni	Z5-002	29.1	6.1	2.8	1.0	49.3	10.9	0.7	39.0	61.0	Low Grade Domain 5
Fungoni	Z5-003	38.1	10.5	3.7	0.7	35.5	10.3	1.2	53.0	47.0	Low Grade Domain 5
Fungoni	Z5-004	35.9	7.9	3.9	0.9	37.1	13.9	0.4	48.6	51.4	Low Grade Domain 5
Fungoni	Z5-005	27.6	9.4	2.6	0.7	44.7	14.5	0.4	40.4	59.6	Low Grade Domain 5
Fungoni	Z5-006	30.8	14.0	2.9	0.8	37.1	13.5	0.9	48.5	51.5	Low Grade Domain 5
Fungoni	Z5-007	34.7	10.0	4.5	0.7	34.7	14.2	1.1	50.0	50.0	Low Grade Domain 5
Fungoni	Z5-008	24.5	7.8	1.7	0.9	37.1	27.5	0.6	34.8	65.2	Low Grade Domain 5
Fungoni	Z5-009	29.5	5.8	2.4	0.6	31.5	30.0	0.3	38.3	61.7	Low Grade Domain 5
Fungoni	Z5-010	32.1	4.9	1.9	1.0	52.7	6.8	0.6	39.9	60.1	Low Grade Domain 5
Fungoni NW	Z5-011	36.8	14.9	5.0	1.7	26.6	13.8	1.2	58.4	41.6	Low Grade Domain 5