



# **STRONG RESULTS FROM ORE RESERVE DRILLING INCREASE RESOURCE CONFIDENCE AND SUPPORT MINE PLANNING AT COBURN**

*Second campaign of Ore Reserve definition drilling successfully completed, with results to underpin updated Resources and Reserves.*

## **HIGHLIGHTS**

- **In-fill drilling has returned significant mineral sands intersections, as well as validating broad, continuous, and often shallow zones of mineralization at Coburn**
- **Significant in-fill drill intersections include:**
  - CBC4945 – 8m @ 4.0% Total Heavy Mineral (THM) from 35m
  - CBC4781 – 3m @ 3.3% THM from 20m
  - CBC4795 – 24m @ 2.8% THM from 26m
  - CBC4939 – 6m @ 2.4% THM from 34m
  - CBC4993 – 12m @ 2.3% THM from 27m
- **A total of 24,892m of Ore Reserve drilling has been completed across 640 drill holes at nominal 125m drill lines and 50m drill hole spacing**
- **This second campaign extends the Ore Reserve definition coverage out to the end of production Year 5, with the results providing additional detail to guide future mine planning**
- **~75% of assaying completed to date, largely confirming Ore Reserve lodes and showing several strong heavy mineral intercepts, both within the 2022 Ore Reserve pit shells (see Figure 3, SECTION B-B') and between pits (see Figure 3, SECTION A-A')**
- **The results will support the next Mineral Resource update and Ore Reserve definition**
- **The Ore Reserve is expected to be updated fully in the March 2024 quarter**

Strandline Resources Limited (ASX: STA) (“Strandline” or the “Company”) is pleased to report strong assay results from its second Ore Reserve definition drilling program, undertaken immediately south of the active mining areas at its Coburn Mineral Sands Project in Western Australia.

**Strandline Managing Director Jozsef Patarica said:** “The drilling has returned significant mineral sands intersections, as well as validating broad, continuous, and often shallow zones of mineralization.

“The Ore Reserve drilling is being undertaken as part of our broader focus on optimisation and improvement initiatives at Coburn, with the objective of providing additional data to assist to help guide our mine planning and scheduling moving forward.



“The drill results reported so far have either met or exceeded our expectations. Encouragingly, we are seeing results that further increase our confidence levels in the existing Mineral Resource as well as some better-than-expected intercepts, both within the 2022 Ore Reserve pit shells and between pits.

“These results will strongly support the next Mineral Resource and Ore Reserve update, which we are aiming to deliver in the March 2024 Quarter.”

The Company is now finalising drill sample assaying which will lead into an updated geological interpretation and mineralogical compositing.

### SUMMARY OF THE IN-FILL DRILLING RESULTS

Coburn Operations are situated in the Gascoyne region of Western Australia, some 250km from the Port of Geraldton. This in-fill air-core drilling program was completed in June this year with a total of 640 holes for 24,892m drilled across the northern areas within the Amy South Mineral Resource and Ore Reserve (on M09/102 and M09/103).

The in-fill drilling campaign targeted production years 3-5 of the Coburn mine plan, which was updated in 2022 following the first in-fill drilling campaign. These latest results will be used to upgrade and optimise the mine plan out to the end of production year five.

The drill results further increase the confidence in the existing Mineral Resource and will provide definitive data for the Ore Reserve.

The in-fill drill program comprised vertical holes completed on a nominal 125m x 50m grid pattern oriented east-west, which is approximately perpendicular to the interpreted ancient coastline and sand dunes. The holes have been drilled to an average depth of 45m with mineralisation generally encountered from close to surface and to the end-of-hole.

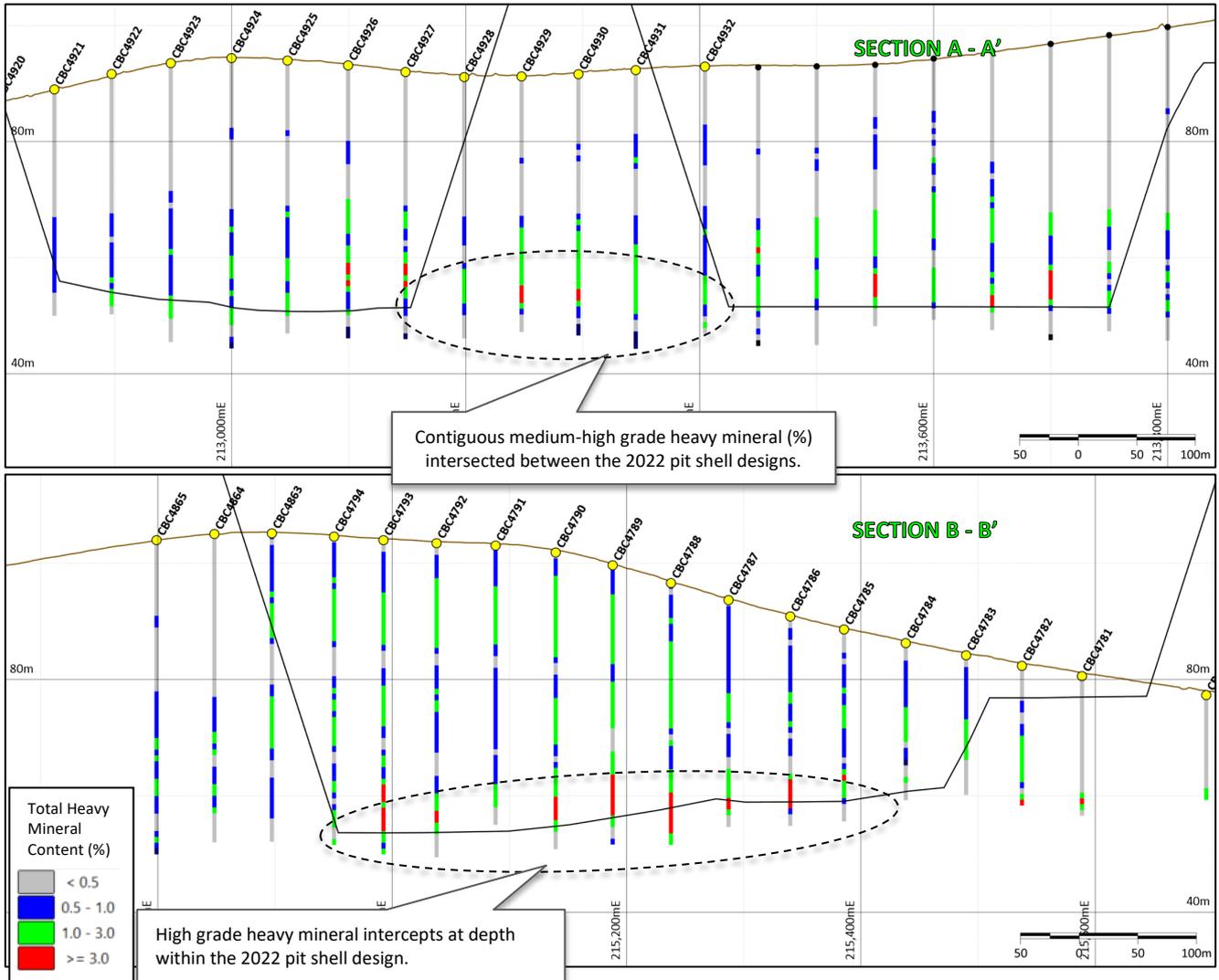
The drilling has delineated broad and continuous intervals of heavy mineral sands along the dunal systems with higher grades encountered below lower-grade sand or overburden.

Significant drill results from this drill program are provided in Table 1 below and a full list of results is provided in Appendix 2.



Figure 1 Coburn Project Drilling





**Figure 4** 2023 Coburn Mine in-fill drill sections A-A' and B-B' (x5 vertical exaggeration) showing the 2022 pit design profiles. Drill hole traces are coloured by total heavy mineral content (%)

This announcement is authorised for release by the Strandline Resources Board of Directors.

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## ABOUT STRANDLINE

Strandline Resources Limited (**ASX: STA**) is an emerging producer of heavy mineral sands with a portfolio of development assets located in Western Australia and within the world's major zircon and titanium producing corridor in East Africa.

Strandline's strategy is to develop and operate high margin, expandable mining assets with market differentiation and global relevance in the sector. Strandline's project portfolio contains high quality assets which offer a range of development options and timelines, geographic diversity and scalability. They include the world-scale Coburn Project in WA and the exciting Tanzanian growth projects including Fungoni and Tajiri.

## FORWARD LOOKING STATEMENTS

This announcement contains certain forward looking statements and comments about future events, including statements about Strandline's expectations about the financial and operating performance of its business. Forward looking statements are only predictions and are subject to risks, uncertainties and assumptions which are outside of the control of Strandline. Forward looking statements can generally be identified by the use of forward looking words including (without limitation) words such as, "expect", "anticipate", "likely", "intend", "should", "could", "may", "predict", "plan", "propose", "will", "believe", "forecast", "estimate", "target" and other similar expressions. These risks, uncertainties and assumptions include (without limitation) commodity prices, currency fluctuations, economic and financial market conditions, environmental risks and legislative, fiscal or regulatory developments, political risks, project delay, approvals and cost estimates. Actual values, results or events may be materially different to those contained in this announcement. Given these uncertainties, readers are cautioned not to place reliance on forward looking statements.

Any forward looking statements in this announcement reflect the views of Strandline only at the date of this announcement. A number of important factors could cause Strandline's actual results to differ materially from the plans, objectives, expectations, estimates and intentions expressed in such forward looking statements. Forward looking statements involve inherent risks and uncertainties, both general and specific and many of which are outside the control of Strandline, and there is a risk that such predictions, forecasts, projections and other forward looking statements will not be achieved. Forward looking statements are provided as a general guide only and should not be relied on as an indication or guarantee of future performance. Subject to any continuing obligations under applicable laws and ASX Listing Rules, Strandline does not undertake any obligation to update or revise any information or any of the forward-looking statements in this announcement to reflect changes in events, conditions or circumstances on which any forward looking statements is based.

## MINERAL SANDS COMPETENT PERSON'S STATEMENTS

The information in this report that relates to Exploration Results is based on, and fairly represents, information and supporting documentation prepared by Mr Gavin Helgeland, Chief Geologist and employee of Strandline. Mr Helgeland is a member of the Australian Institute of Geoscientists and he has sufficient experience which is relevant to the style of mineralisation and type of deposits under consideration and to the activity which has been undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Helgeland consents to the inclusion in this release of the matters based on the information in the form and context in which they appear.

The information in this report that relates to Mineral Resources is based on, and fairly represents, information and supporting documentation prepared by Mr Greg Jones, (Consultant to Strandline and Geological Services Manager for IHC Robbins) and Mr Brendan Cummins (Consulting Geologist of Strandline). Mr Jones is a member of the Australian Institute of Mining and Metallurgy and Mr Cummins is a member of the Australian Institute of Geoscientists and both have sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration, and to the activities undertaken to qualify as Competent Persons as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Specifically, Mr Cummins is the Competent Person for the provision of the drill database, and completed the site inspection. Mr Jones is the Competent Person for the data integration and resource estimation. Mr Jones and Mr Cummins consent to the inclusion in this report of the matters based on their information in the form and context in which they appear.

The information in this report that relates to the Coburn Ore Reserves is based on information compiled under the direction of Mr Adrian Jones. Mr Jones is a Member of the Australasian Institute of Mining and Metallurgy and is employed by AMC. Mr Jones has sufficient experience relevant to the style of mineralization and type of deposit under consideration to qualify as a Competent Person as defined in the JORC Code. Non mining modifying factors for the Ore Reserve estimate are drawn from contributions provided by various sources. Significant contributors to this report are identified in Table 5 (ASX announcement 16 April 2019) together with their area of contribution.

In relation to the Mineral Resource announced on 16 April 2019 for the Coburn Project, the Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and that all material assumptions and technical parameters underpinning the estimates in that market announcement continue to apply and have not materially changed.

## APPENDIX 1 - JORC TABLE 1

### Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>Aircore drilling was used to obtain samples for analysis at 1m intervals</li> <li>Each 1m sample was homogenized within the sample bag by rotating the sample bag</li> <li>A sample of sand, approx. 100gm, is scooped from the sample bag for an initial visual THM% estimation and logging. A similar sample mass is used for every pan sample for visual THM% estimation</li> <li>The standard sized sample is to ensure calibration is maintained for consistency in visual estimation</li> <li>A sample ledger is kept at the drill rig for recording sample numbers</li> <li>The 1m aircore drill samples have an average range between 5kg and 8kg and were split down using a rig based rotary splitter to 1.5 to 2.5kg.</li> <li>The laboratory sample was dried and processed further.</li> <li>The plus 3.3mm larger oversize is screened and weighed.</li> <li>Approximately 100gm of the sand sample was then split from the original sample using a micro riffle splitter or rotary splitter that is processed further with de-sliming (removal of -45µm fraction) and removal of oversize (+710µm fraction)</li> <li>The remaining sand is then used for heavy liquid separation using funnels and TBE to determine total heavy mineral (THM) content</li> </ul>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<ul style="list-style-type: none"> <li>Aircore drilling with inner tubes for sample return was used</li> <li>Aircore is considered a standard industry technique for HMS mineralization. Aircore drilling is a form of reverse circulation drilling where the sample is collected at the face and returned inside the inner tube</li> <li>Aircore drill rods used were 3m long</li> <li>NQ diameter (76mm) drill bits and rods were used</li> <li>All drill holes were vertically</li> </ul>
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<ul style="list-style-type: none"> <li>AC drill sample recovery is monitored by reviewing the sample mass of the total weight of the 1m interval weighed at the laboratory</li> <li>Industry leading mineral sand drilling specialists were engaged to drill the holes with experienced drillers to maximize drill recovery such as maintaining drill penetration rates, airflow and water injection</li> <li>Samples were not weighed at the rig</li> <li>While initially collaring the hole, limited sample recovery can occur in the initial 0.0m to 2m sample interval owing to sample and air loss into the surrounding loose soils</li> <li>The initial 0m to 2m sample interval is drilled very slowly in order to achieve optimum sample recovery</li> <li>The entire 1m sample passes through the on board rotary splitter and the 1m sample collected in a</li> </ul>

Criteria	JORC Code explanation	Commentary
		<p>pre-numbered calico. The bulk reject is not collected and is shoveled back down the hole upon completion</p> <ul style="list-style-type: none"> <li>• About 10 1m samples are placed in a number poly weaves and secured with a cable tie</li> <li>• Wet samples were rarely recorded in the ore zones with water encountered at the end of the hole in the unmineralized basement (clays)</li> <li>• At the end of each drill rod, the drill string is cleaned by blowing down with air/water to remove any clay and silt potentially built up in the sample pipes</li> <li>• The twin-tube aircore drilling technique is known to provide high quality samples from the face of the drill hole</li> </ul>
Logging	<ul style="list-style-type: none"> <li>• Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>• Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</li> <li>• The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>• The 1m aircore samples were each qualitatively logged using a field laptop (Toughbook) an entered into Microsoft Excel logsheet</li> <li>• The aircore samples were logged for lithology, colour, grainsize, rounding, hardness, sorting, estimated THM%, estimated Slimes% and any relevant comments</li> <li>• Every drillhole was logged in full with detailed logging based on a small sample of sand taken from the split sample to improve representivity</li> <li>• Logging is undertaken with reference to a Drilling Guideline with codes prescribed and guidance on description to ensure consistent and systematic data collection</li> </ul>
Sub-sampling techniques and sample preparation	<ul style="list-style-type: none"> <li>• If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>• If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>• For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>• Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>• Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>• Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul style="list-style-type: none"> <li>• The 1m AC drill sample collected at the source was split down to 1.5 to 2.5kg using a rig based rotary splitter</li> <li>• The sample sizer and process is considered an appropriate technique for mineral sands</li> <li>• The sample sizes were deemed suitable to reliably capture THM, slime, and oversize characteristics, based on industry experience of the geologists involved and consultation with laboratory staff</li> <li>• Field duplicates of the samples were completed at a frequency of 1 per 40 primary samples</li> <li>• Standard Reference Material samples are inserted into the sample stream in the field at a frequency of 1 per 40 samples</li> </ul>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>• For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>• Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</li> </ul>	<ul style="list-style-type: none"> <li>• The wet panning at the drill site provides an estimate of the THM% which is sufficient for the purpose of determining approximate concentrations of THM in the first instance</li> </ul> <p>Aircore sample:</p> <ul style="list-style-type: none"> <li>• The individual 1m aircore sub-samples (approx. 2000g) were analysed by Western Geolabs and Diamantina Laboratories in Perth, Western Australia</li> <li>• Both laboratories are considered the Primary laboratories but 1/40 samples from each primary laboratory batch were split and sent to the other laboratory for secondary analysis</li> <li>• The 2kg samples are dried first screened to remove +3.3mm fraction. A 100g sub sample was then washed to remove Slimes (-45µm), screened for Oversize (+710 µm). The remaining sand samples are analysed for total heavy mineral (-1mm to</li> </ul>

Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>+45µm) content using heavy liquid separation</li> <li>The laboratory used TBE as the heavy liquid medium – with density range between 2.92 and 2.96 g/ml</li> <li>This is an industry standard technique</li> <li>Field duplicates and HM Standards are alternatively inserted into the sample string at a frequency of 1 per 40 primary samples</li> <li>Western Geolabs completed its own internal QA/QC checks that included laboratory repeats every 10th sample prior to the results being released</li> <li>Diamantina completed its own internal QA/QC checks that included laboratory repeats and the insertion of standard reference material prior to the results being released</li> <li>Analysis of QA/QC samples show the laboratory data to be of acceptable accuracy and precision.</li> <li>Any batches that failed QAQC validation were repeated in total</li> <li>The adopted QA/QC protocols are acceptable and equal to or better than Industry Standard</li> </ul>
<p>Verification of sampling and assaying</p>	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>All results are checked by the Chief Geologist, in addition to the independent consulting Resource Geologist when appropriate</li> <li>The Chief Geologist and independent Resource geologist make periodic visits to the laboratory to observe sample processing</li> <li>A process of laboratory data validation using mass balance is undertaken to identify entry errors or questionable data</li> <li>Field and laboratory duplicate data pairs (THM/oversize/slime) of each batch are plotted to identify potential quality control issues</li> <li>Standard Reference Material sample results are checked from each sample batch to ensure they are within tolerance (&lt;2SD) and that there is no bias</li> <li>The field and laboratory data has been updated into a master spreadsheet and then uploaded into Micromine files.</li> <li>Data validation criteria are included to check for overlapping sample intervals, end of hole match between 'Lithology', 'Sample', 'Survey' files, duplicate sample numbers and other common errors</li> <li>No adjustments are made to the primary assay data</li> </ul>
<p>Location of data points</p>	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>Specification of the grid system used.</li> <li>Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>Down hole surveys for shallow aircore holes are not required</li> <li>A handheld GPS was initially used to identify the positions of the drill holes in the field. The handheld GPS has an accuracy of +/- 5m in the horizontal</li> <li>The datum used is GDA94 and coordinates are projected as UTM zone 50S</li> <li>After the drill program was completed the drill collar locations were surveyed using highly accurate (+/- 10mm X, Y, Z) Differential GPS.</li> <li>The accuracy of the DGPS locations is considered appropriate for this stage of resource development</li> </ul>

Criteria	JORC Code explanation	Commentary
<i>Data spacing and distribution</i>	<ul style="list-style-type: none"> <li>• <i>Data spacing for reporting of Exploration Results.</i></li> <li>• <i>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</i></li> <li>• <i>Whether sample compositing has been applied.</i></li> </ul>	<p>Aircore Drilling</p> <ul style="list-style-type: none"> <li>• The previous drill density was 100 x 500m which was reduced to 50 x 125m</li> <li>• This spacing is designed for detailed infill and appropriate for Mineral Resource Estimation and increasing the resource classification</li> <li>• Each aircore drill sample is a single 1m sample of sand intersected down the hole</li> <li>• No compositing has been applied to models for values of THM, slime and oversize</li> <li>• Compositing of heavy samples was undertaken the HM concentrates for mineral assemblage determination.</li> </ul>
<i>Orientation of data in relation to geological structure</i>	<ul style="list-style-type: none"> <li>• <i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i></li> <li>• <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The aircore drilling was oriented perpendicular to the strike of mineralization defined by drilling data at 360°</li> <li>• The strike of the mineralization is sub-parallel to the contemporary coastline and is known to be relatively well controlled</li> <li>• Drill holes were vertical because the nature of the mineralisation is relatively horizontal</li> <li>• The orientation of the drilling is considered appropriate for testing the lateral and vertical extent of mineralization limiting bias</li> </ul>
<i>Sample security</i>	<ul style="list-style-type: none"> <li>• <i>The measures taken to ensure sample security.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Aircore samples remained in the custody of Company representatives until they were trucked to Perth using an independent contractor</li> <li>• The samples were transported to Perth and delivered directly to the laboratory</li> <li>• The laboratory inspected the packages and did not report tampering of the samples</li> </ul>
<i>Audits or reviews</i>	<ul style="list-style-type: none"> <li>• <i>The results of any audits or reviews of sampling techniques and data.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Internal reviews were undertaken</li> </ul>

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
<i>Mineral tenement and land tenure status</i>	<ul style="list-style-type: none"> <li>• <i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i></li> <li>• <i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The exploration work was completed on tenements that are 100% owned by Strandline Resource through 100% owned Coburn Resources</li> <li>• The drill samples were taken from tenement ML 09/102 and ML 09/103,</li> <li>• A Mining Agreement is in place with the Traditional Owners and ML 09/102 and ML 09/103 was surveyed for archaeology and ethnography in 2023</li> <li>• A 100m buffer to the Shark Bay World Heritage Property is located within M09/102 and ML 09/103 along the western boundary</li> </ul>
<i>Exploration done by other parties</i>	<ul style="list-style-type: none"> <li>• <i>Acknowledgment and appraisal of exploration by other parties.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The Coburn deposits were discovered by Strandline Resources (formerly Gunson Resources) in 2002</li> <li>• Prior to the Company discovering the Coburn deposit there was limited exploration undertaken by third parties</li> </ul>
<i>Geology</i>	<ul style="list-style-type: none"> <li>• <i>Deposit type, geological setting and style of mineralisation.</i></li> </ul>	<ul style="list-style-type: none"> <li>•</li> </ul>
<i>Drill hole Information</i>	<ul style="list-style-type: none"> <li>• <i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:</i> <ul style="list-style-type: none"> <li>○ <i>easting and northing of the drill hole collar</i></li> <li>○ <i>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</i></li> <li>○ <i>dip and azimuth of the hole</i></li> <li>○ <i>down hole length and interception depth</i></li> <li>○ <i>hole length.</i></li> </ul> </li> <li>• <i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i></li> </ul>	<ul style="list-style-type: none"> <li>• The drill hole data are reported in Appendix 2.</li> </ul>
<i>Data aggregation methods</i>	<ul style="list-style-type: none"> <li>• <i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</i></li> <li>• <i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i></li> <li>• <i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i></li> </ul>	<ul style="list-style-type: none"> <li>• All length weighted intervals are reported for each hole in (Appendix 2) for grades above 0.8% THM</li> </ul>

Criteria	JORC Code explanation	Commentary
<i>Relationship between mineralisation widths and intercept lengths</i>	<ul style="list-style-type: none"> <li>• <i>These relationships are particularly important in the reporting of Exploration Results.</i></li> <li>• <i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i></li> <li>• <i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').</i></li> </ul>	<ul style="list-style-type: none"> <li>• The nature of the mineralisation is broadly horizontal, thus vertical aircore holes are thought to represent close to true thicknesses of the mineralisation</li> <li>• Downhole widths are reported</li> </ul>
<i>Diagrams</i>	<ul style="list-style-type: none"> <li>• <i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Figures and plans are displayed in the main text of the Release</li> </ul>
<i>Balanced reporting</i>	<ul style="list-style-type: none"> <li>• <i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i></li> </ul>	<ul style="list-style-type: none"> <li>• All drill results &gt; 0.8% THM have been reported and tabulated in Appendix 2.</li> </ul>
<i>Other substantive exploration data</i>	<ul style="list-style-type: none"> <li>• <i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Mineral assemblage test work is substantially advanced and will be required to update the Mineral Resource Estimate</li> <li>• Bulk metallurgical test work was previously undertaken in 2019 and 2020 on a number of representative samples across the deposit</li> </ul>
<i>Further work</i>	<ul style="list-style-type: none"> <li>• <i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</i></li> <li>• <i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i></li> </ul>	<ul style="list-style-type: none"> <li>• Further infill aircore drilling is planned to continue drilling out resources to update the Mineral Resource that will feed into Ore Reserves and then updates to the mine plan and mine schedules</li> <li>• More detailed mineral assemblage studies are being completed on the mineral concentrates.</li> <li>• The results will be used to update and expand the current JORC MRE for the Amy South Mineral Sands Deposit.</li> </ul>

APPENDIX 2 - COBURN AMY SOUTH INFILL DRILL RESULTS TO DATE

Hole Id	East (GDA94)	North (GDA94)	RL	DIP	AZIMUTH	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIMES (%)	OS (%)	YEAR
CBC4781	215600	7048775	75.7197	-90	0	24	20	23	3	3.3	47.4	14.5	2023
CBC4782	215550	7048775	77.3139	-90	0	24	12	24	12	1.5	10.6	5.6	2023
CBC4783	215500	7048775	79.1676	-90	0	24	9	18	9	1.4	2.4	0.4	2023
CBC4784	215450	7048775	81.0942	-90	0	27	4	24	20	1.3	2.9	1.5	2023
CBC4785	215400	7048775	83.3124	-90	0	33	10	30	20	1.3	3.5	0.3	2023
CBC4786	215350	7048775	85.6592	-90	0	36	10	33	23	1.9	3.0	0.5	2023
CBC4787	215300	7048775	87.8413	-90	0	39	7	37	30	1.5	2.7	0.4	2023
CBC4788	215250	7048775	90.5047	-90	0	45	2	45	43	2.1	3.0	0.3	2023
CBC4789	215200	7048775	93.4547	-90	0	48	4	45	41	2.2	1.7	0.3	2023
CBC4790	215150	7048775	96.6504	-90	0	51	2	48	46	1.7	2.5	0.2	2023
CBC4791	215100	7048775	99.069	-90	0	48	3	45	42	1.1	2.8	0.7	2023
CBC4792	215050	7048775	100.29	-90	0	54	4	50	46	1.4	2.0	0.2	2023
CBC4793	215000	7048775	100.62	-90	0	54	7	54	47	1.7	2.8	0.2	2023
CBC4794	214950	7048775	101.2787	-90	0	53	2	53	51	1.2	3.3	0.5	2023
CBC4795	214976.28	7048654.8	102.6349	-90	0	54	26	50	24	2.8	2.0	0.2	2023
CBC4796	215076.28	7048654.8	101.9748	-90	0	51	4	48	44	1.5	1.6	0.1	2023
CBC4797	215176.28	7048654.8	98.0048	-90	0	48	5	45	40	1.0	2.5	0.4	2023
CBC4798	215276.28	7048654.8	92.1888	-90	0	42	10	42	32	2.1	3.0	0.1	2023
CBC4799	215375.91	7048652.3	87.2918	-90	0	35	10	35	25	1.2	10.4	0.5	2023
CBC4800	215475.74	7048652.1	83.8735	-90	0	33	8	31	23	1.4	5.3	1.7	2023
CBC4801	215586.85	7048651.4	80.5394	-90	0	27	6	26	20	1.0	6.7	3.2	2023
CBC4802	215650	7048650	79.2034	-90	0	27	10	20	10	0.9	3.8	0.9	2023
CBC4804	215550	7048525	82.5985	-90	0	27	4	20	16	1.9	4.7	3.9	2023
CBC4805	215499.94	7048521.5	83.2312	-90	0	30	0	29	29	1.7	7.6	2.2	2023
CBC4806	215449.94	7048521.5	84.2966	-90	0	33	5	22	17	1.7	3.3	1.9	2023
CBC4807	215399.94	7048521.5	85.8234	-90	0	33	8	33	25	1.5	7.0	1.2	2023
CBC4808	215349.94	7048521.5	87.7145	-90	0	36	8	36	28	1.4	4.0	1.6	2023
CBC4809	215299.94	7048521.5	89.9168	-90	0	39	12	36	24	1.6	2.0	0.2	2023
CBC4810	215249.94	7048521.5	92.5691	-90	0	42	4	42	38	1.8	3.6	0.5	2023
CBC4811	215199.94	7048521.5	95.4083	-90	0	48	3	45	42	1.2	2.3	0.4	2023
CBC4812	215149.94	7048521.5	98.2872	-90	0	50	3	48	45	1.2	1.9	0.5	2023
CBC4813	215099.94	7048521.5	100.7998	-90	0	51	9	48	39	1.2	1.8	0.1	2023
CBC4814	215049.94	7048521.5	102.2801	-90	0	52	16	46	30	1.1	1.9	0.2	2023
CBC4815	214999.94	7048521.5	102.8042	-90	0	51	10	48	38	1.1	2.9	0.2	2023
CBC4816	214950	7048525	102.713	-90	0	54	21	42	21	1.2	2.3	0.2	2023
CBC4817	215874.47	7048146.1	87.1738	-90	0	24	10	22	12	1.1	23.1	12.0	2023
CBC4818	215775.46	7048152.1	78.2491	-90	0	21	2	15	13	1.2	5.6	4.2	2023
CBC4819	215675.96	7048147.6	79.82	-90	0	24	2	23	21	1.6	7.8	3.1	2023
CBC4820	215575.65	7048149.8	81.5652	-90	0	27	12	27	15	0.9	11.9	2.0	2023
CBC4821	215475.46	7048152.1	84.6435	-90	0	32	9	25	16	1.4	3.1	0.7	2023
CBC4822	215375.46	7048152.1	88.8478	-90	0	36	11	29	18	1.4	3.0	0.3	2023
CBC4823	215275.46	7048152.1	92.3969	-90	0	39	10	34	24	1.3	2.9	0.4	2023

Hole Id	East (GDA94)	North (GDA94)	RL	DIP	AZIMUTH	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIMES (%)	OS (%)	YEAR
CBC4824	215175.75	7048153.6	87.1738	-90	0	43	15	38	23	1.7	2.1	0.1	2023
CBC4825	215750	7048525	79.8334	-90	0	23	8	21	13	1.2	2.7	0.7	2023
CBC4826	215700	7048525	81.2249	-90	0	25	5	25	20	1.1	7.9	1.2	2023
CBC4827	215650	7048525	82.1149	-90	0	26	2	26	24	1.1	7.2	3.0	2023
CBC4828	215600	7048525	82.5712	-90	0	26	1	18	17	1.3	4.0	2.2	2023
CBC4829	214950	7048400	102.2103	-90	0	51	16	47	31	1.1	3.0	0.3	2023
CBC4830	215000	7048400	102.6918	-90	0	54	16	54	38	1.4	14.4	6.2	2023
CBC4831	215050	7048400	101.9355	-90	0	54	17	54	37	1.2	12.3	7.3	2023
CBC4832	215100	7048400	100.0306	-90	0	51	6	51	45	1.1	3.5	1.3	2023
CBC4833	215150	7048400	97.6043	-90	0	48	8	42	34	1.1	2.7	0.2	2023
CBC4834	215200	7048400	95.0358	-90	0	46	15	36	21	1.1	2.8	0.1	2023
CBC4835	215250	7048400	92.2507	-90	0	43	8	42	34	1.7	6.3	1.3	2023
CBC4836	215300	7048400	89.548	-90	0	39	12	38	26	1.6	4.9	1.3	2023
CBC4837	215350	7048400	87.1399	-90	0	36	25	29	4	1.2	2.4	0.4	2023
CBC4838	215400	7048400	84.8709	-90	0	33	5	31	26	1.3	4.9	3.1	2023
CBC4839	215450	7048400	82.8237	-90	0	27	3	23	20	1.5	3.7	2.7	2023
CBC4840	215500	7048400	81.218	-90	0	27	3	26	23	1.3	8.5	3.9	2023
CBC4841	215550	7048400	80.1346	-90	0	25	10	24	14	1.2	10.5	6.3	2023
CBC4842	215600	7048400	79.4635	-90	0	24	13	23	10	1.5	12.5	13.5	2023
CBC4843	215650	7048400	79.2803	-90	0	24	7	23	16	1.8	10.5	4.8	2023
CBC4844	215700	7048400	79.0827	-90	0	24	3	17	14	1.3	3.8	1.9	2023
CBC4845	215750	7048400	78.3489	-90	0	24	2	20	18	1.1	3.2	1.8	2023
CBC4846	215800	7048400	77.334	-90	0	21	2	17	15	0.9	4.7	0.7	2023
CBC4847	215100	7048275	99.0193	-90	0	52	12	50	38	1.3	4.5	5.7	2023
CBC4848	215150	7048275	96.6016	-90	0	48	34	37	3	1.3	2.4	0.1	2023
CBC4849	215200	7048275	94.2788	-90	0	45	13	44	31	1.5	5.4	1.2	2023
CBC4850	215250	7048275	92.0111	-90	0	45	15	39	24	1.9	2.9	0.4	2023
CBC4851	215300	7048275	89.608	-90	0	39	13	38	25	1.6	5.2	3.0	2023
CBC4852	215350	7048275	87.0482	-90	0	36	12	35	23	1.7	12.8	2.7	2023
CBC4853	215400	7048275	84.6677	-90	0	33	11	33	22	1.5	10.2	3.9	2023
CBC4854	215450	7048275	82.4306	-90	0	29	6	28	22	1.7	6.6	3.1	2023
CBC4855	215500	7048275	80.7733	-90	0	27	9	20	11	1.2	4.9	2.9	2023
CBC4856	215550	7048275	79.4938	-90	0	26	11	18	7	1.0	4.1	1.1	2023
CBC4857	215600	7048275	78.4203	-90	0	24	15	22	7	1.2	15.4	11.7	2023
CBC4858	215650	7048275	77.7162	-90	0	24	12	23	11	1.2	23.6	4.7	2023
CBC4859	215700	7048275	76.764	-90	0	21	7	15	8	1.6	5.6	3.1	2023
CBC4860	215750	7048275	75.728	-90	0	21	7	20	13	1.5	8.8	7.3	2023
CBC4861	215800	7048275	74.5297	-90	0	21	9	19	10	1.1	9.8	2.0	2023
CBC4863	214900	7048775	102.147	-90	0	53	8	49	41	1.1	2.9	0.3	2023
CBC4864	214850	7048775	102.6256	-90	0	53	33	48	15	1.0	2.1	0.2	2023
CBC4865	214800	7048775	102.5168	-90	0	54	29	52	23	1.0	5.1	2.5	2023
CBC4866	214875.9	7048649.6	102.7427	-90	0	54	15	50	35	1.2	3.8	0.1	2023
CBC4867	214775.9	7048649.6	100.979	-90	0	51	7	51	44	1.1	4.7	1.5	2023

Hole Id	East (GDA94)	North (GDA94)	RL	DIP	AZIMUTH	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIMES (%)	OS (%)	YEAR
CBC4868	214675.9	7048649.6	98.1916	-90	0	46	2	42	40	1.3	3.4	0.2	2023
CBC4869	214575.9	7048649.6	97.3202	-90	0	50	14	48	34	1.0	5.9	1.1	2023
CBC4870	214475.9	7048649.6	98.3504	-90	0	49	4	45	41	1.3	3.2	0.2	2023
CBC4871	214900	7048525	102.2897	-90	0	54	21	51	30	1.1	7.8	1.8	2023
CBC4872	214850	7048525	102.1005	-90	0	52	22	46	24	1.2	3.8	0.3	2023
CBC4873	214900	7048400	101.5187	-90	0	48.8	16	40	24	1.1	2.5	0.3	2023
CBC4874	214850	7048400	87.1738	-90	0	48.1	18	39	21	1.1	2.0	0.3	2023
CBC4875	214800	7048400	87.1738	-90	0	51	18	49	31	1.2	6.7	8.8	2023
CBC4876	214750	7048400	87.1738	-90	0	49	18	25	7	1.3	2.9	0.1	2023
CBC4877	214700	7048400	87.1738	-90	0	51	13	40	27	0.9	2.9	0.1	2023
CBC4878	214650	7048400	87.1738	-90	0	48	21	29	8	1.0	2.7	0.2	2023
CBC4879	214600	7048400	87.1738	-90	0	48	20	45	25	1.1	4.4	0.3	2023
CBC4880	214550	7048400	87.1738	-90	0	48	22	45	23	1.2	3.3	0.5	2023
CBC4881	214500	7048400	87.1738	-90	0	47	34	44	10	1.1	2.1	0.1	2023
CBC4882	212476.53	7049136.1	85.075	-90	0	46	21	31	10	1.7	1.7	0.4	2023
CBC4883	212576.53	7049136.1	86.3156	-90	0	38.4	18	35	17	1.7	2.0	0.8	2023
CBC4885	212776.53	7049136.1	89.759	-90	0	42	36	39	3	1.2	1.4	0.4	2023
CBC4886	212876.53	7049136.1	90.4442	-90	0	50	26	43	17	1.1	2.5	1.8	2023
CBC4887	212976.53	7049136.1	89.0553	-90	0	48	20	44	24	1.6	4.0	1.2	2023
CBC4888	213076.53	7049136.1	86.7938	-90	0	42	21	42	21	2.1	7.3	0.5	2023
CBC4889	213176.53	7049136.1	84.6744	-90	0	42	20	34	14	1.4	2.5	0.6	2023
CBC4890	213276.53	7049136.1	84.0987	-90	0	39	25	37	12	1.4	3.3	0.5	2023
CBC4891	213376.53	7049136.1	85.3093	-90	0	41	16	34	18	1.1	1.5	0.4	2023
CBC4892	213476.53	7049136.1	88.699	-90	0	44	34	35	1	1.0	2.5	0.1	2023
CBC4893	212400	7049275	83.5851	-90	0	42	17	29	12	1.1	1.8	1.0	2023
CBC4894	212450	7049275	85.3111	-90	0	39	24	35	11	1.2	1.8	0.4	2023
CBC4895	212500	7049275	86.8187	-90	0	42	24	35	11	1.6	2.0	1.1	2023
CBC4896	212550	7049275	88.368	-90	0	40	26	37	11	1.2	1.8	0.4	2023
CBC4897	212600	7049275	89.9678	-90	0	42	38	41	3	1.1	3.8	0.9	2023
CBC4898	212650	7049275	90.9948	-90	0	41.3	41	41.3	0.3	0.8	3.2	7.2	2023
CBC4899	212700	7049275	91.2672	-90	0	43.1	38	43	5	1.1	2.6	1.9	2023
CBC4900	212750	7049275	91.2082	-90	0	48	25	44	19	1.1	2.6	2.0	2023
CBC4901	212850	7049275	90.5137	-90	0	45	12	45	33	1.2	4.0	4.6	2023
CBC4902	212900	7049275	89.7356	-90	0	46.5	10	44	34	1.1	2.2	1.1	2023
CBC4903	212950	7049275	88.5869	-90	0	46	10	43	33	1.1	4.2	0.9	2023
CBC4904	213000	7049275	86.8306	-90	0	44.1	10	43	33	1.4	4.7	0.8	2023
CBC4905	213050	7049275	85.1402	-90	0	40	19	37	18	1.8	2.3	0.4	2023
CBC4906	213100	7049275	83.6944	-90	0	39	20	32	12	1.2	2.2	0.1	2023
CBC4907	213150	7049275	82.5243	-90	0	39	18	31	13	1.1	2.2	0.4	2023
CBC4908	213200	7049275	81.8673	-90	0	35	27	28	1	0.8	2.7	0.2	2023
CBC4909	213250	7049275	81.9671	-90	0	36	28	29	1	0.8	2.9	0.3	2023
CBC4910	212800	7049275	90.9182	-90	0	48	24	46	22	1.4	3.0	3.4	2023
CBC4911	213300	7049275	82.8517	-90	0	38	28	30	2	0.9	1.0	0.2	2023

Hole Id	East (GDA94)	North (GDA94)	RL	DIP	AZIMUTH	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIMES (%)	OS (%)	YEAR
CBC4912	213350	7049275	84.2595	-90	0	39	28	31	3	1.6	1.8	0.1	2023
CBC4913	212450	7049025	84.9184	-90	0	32.1	15	25	10	1.1	2.4	0.8	2023
CBC4914	212500	7049025	85.0966	-90	0	36.1	16	27	11	1.6	2.4	1.1	2023
CBC4915	212550	7049025	84.1525	-90	0	42	19	33	14	1.1	3.5	1.8	2023
CBC4916	212600	7049025	82.9433	-90	0	39	16	26	10	1.3	2.6	1.5	2023
CBC4917	212650	7049025	82.6972	-90	0	36	16	26	10	1.6	3.1	2.1	2023
CBC4918	212700	7049025	83.7026	-90	0	30.8	17	27	10	1.2	2.1	1.3	2023
CBC4919	212750	7049025	85.4999	-90	0	37	18	27	9	1.0	2.5	1.8	2023
CBC4920	212800	7049025	87.7765	-90	0	40	21	29	8	0.9	4.8	0.6	2023
CBC4921	212850	7049025	89.8389	-90	0	39	34	35	1	0.9	5.0	8.0	2023
CBC4922	212900	7049025	91.4386	-90	0	41.4	34	40	6	1.1	2.6	3.9	2023
CBC4923	212950	7049025	92.0165	-90	0	48	29	44	15	1.3	2.8	2.1	2023
CBC4924	213000	7049025	91.1443	-90	0	50	26	49	23	1.2	6.7	3.8	2023
CBC4925	213050	7049025	89.9282	-90	0	47	26	44	18	1.3	2.3	0.9	2023
CBC4926	213100	7049025	88.77	-90	0	47	23	43	20	1.8	2.7	1.1	2023
CBC4927	213150	7049025	87.9514	-90	0	46	23	42	19	1.9	2.8	0.9	2023
CBC4928	213200	7049025	87.8357	-90	0	45	33	39	6	2.1	2.0	0.2	2023
CBC4929	213250	7049025	88.1267	-90	0	44	25	40	15	2.1	3.1	0.7	2023
CBC4930	213300	7049025	88.7293	-90	0	45	25	41	16	1.9	3.7	0.7	2023
CBC4931	213350	7049025	89.2704	-90	0	48	14	43	29	1.3	2.8	0.6	2023
CBC4932	213400	7049025	89.7314	-90	0	46	15	45	30	1.3	3.1	0.7	2023
CBC4933	212400	7049025	84.1563	-90	0	42	16	37	21	1.0	2.2	1.7	2023
CBC4934	213400	7049275	86.0818	-90	0	40	12	36	24	2.2	2.1	0.1	2023
CBC4935	213450	7049275	88.2224	-90	0	44	31	42	11	2.3	2.2	0.2	2023
CBC4936	213500	7049275	90.3591	-90	0	48	17	42	25	1.6	2.4	0.1	2023
CBC4937	213500	7049275	90.3591	-90	0	48	32	41	9	2.2	3.1	0.1	2023
CBC4938	213850	7048400	91.1744	-90	0	42	24	41	17	2.2	2.7	0.1	2023
CBC4939	213900	7048400	91.4961	-90	0	42	34	40	6	2.4	2.8	0.1	2023
CBC4940	213900	7048275	95.9756	-90	0	52	42	46	4	1.8	3.3	0.0	2023
CBC4941	213950	7048275	87.1738	-90	0	48	30	45	15	1.7	4.7	0.2	2023
CBC4942	213950	7048400	92.2282	-90	0	47	35	41	6	1.6	1.9	0.1	2023
CBC4943	214000	7048400	92.7078	-90	0	47	38	42	4	1.3	2.2	0.1	2023
CBC4944	214050	7048400	92.8637	-90	0	48	33	45	12	1.3	2.9	0.4	2023
CBC4945	214100	7048400	92.8304	-90	0	47	35	43	8	4.0	2.0	0.1	2023
CBC4946	214150	7048400	87.1738	-90	0	46	36	42	6	1.4	2.8	0.1	2023
CBC4947	212450	7048900	81.409	-90	0	33	10	20	10	1.0	1.5	1.6	2023
CBC4948	212500	7048900	82.2724	-90	0	30	11	21	10	1.1	3.2	1.7	2023
CBC4949	212550	7048900	81.0356	-90	0	31	16	22	6	1.2	2.7	1.3	2023
CBC4950	212600	7048900	79.0955	-90	0	31	13	29	16	1.2	4.9	1.5	2023
CBC4951	212650	7048900	77.9192	-90	0	32	15	26	11	1.1	4.0	1.7	2023
CBC4952	212700	7048900	78.0816	-90	0	30	14	22	8	1.2	7.3	2.6	2023
CBC4953	212750	7048900	79.7304	-90	0	32	11	25	14	1.4	3.8	1.0	2023
CBC4954	212800	7048900	82.4082	-90	0	33	6	25	19	1.3	4.0	1.0	2023

Hole Id	East (GDA94)	North (GDA94)	RL	DIP	AZIMUTH	EOH (m)	FROM (m)	TO (m)	INTERVAL (m)	THM (%)	SLIMES (%)	OS (%)	YEAR
CBC4955	212850	7048900	85.2695	-90	0	41	17	28	11	1.0	3.6	1.1	2023
CBC4956	212900	7048900	88.3366	-90	0	42	20	34	14	1.0	3.0	1.1	2023
CBC4957	212950	7048900	91.0139	-90	0	43	14	41	27	1.7	2.7	1.1	2023
CBC4958	213000	7048900	92.271	-90	0	48	12	44	32	1.3	2.9	0.7	2023
CBC4959	213050	7048900	92.5567	-90	0	50	29	49	20	1.2	5.0	3.2	2023
CBC4960	213100	7048900	92.0986	-90	0	47	29	47	18	1.0	4.5	1.6	2023
CBC4961	213150	7048900	91.4839	-90	0	49	31	45	14	1.0	2.7	1.5	2023
CBC4962	213200	7048900	91.0057	-90	0	50	36	40	4	1.4	2.2	0.9	2023
CBC4963	213250	7048900	90.9716	-90	0	48	37	40	3	1.2	2.0	2.0	2023
CBC4964	213300	7048900	91.5379	-90	0	45	34	40	6	1.1	2.5	0.3	2023
CBC4966	213250	7048775	92.442	-90	0	51	42	45	3	1.1	3.7	4.8	2023
CBC4967	213200	7048775	93.1712	-90	0	48	42	46	4	1.1	3.5	7.1	2023
CBC4968	213150	7048775	94.0068	-90	0	52	43	48	5	1.2	2.8	5.3	2023
CBC4969	213100	7048775	94.5746	-90	0	49	41	48	7	1.2	1.8	2.2	2023
CBC4970	213050	7048775	94.5878	-90	0	48	35	46	11	1.4	1.8	1.3	2023
CBC4971	213000	7048775	93.4381	-90	0	47	37	41	4	0.9	1.1	0.7	2023
CBC4972	212950	7048775	91.0788	-90	0	41	24	39	15	1.3	2.9	3.7	2023
CBC4973	212900	7048775	87.8889	-90	0	37	20	35	15	1.2	3.1	5.9	2023
CBC4974	212850	7048775	84.3799	-90	0	37	17	29	12	1.3	2.6	1.6	2023
CBC4975	212800	7048775	81.2384	-90	0	36	14	23	9	1.2	3.0	2.6	2023
CBC4976	212750	7048775	78.874	-90	0	35	14	23	9	1.1	2.1	4.5	2023
CBC4977	212700	7048775	77.557	-90	0	35	13	23	10	1.4	1.6	2.1	2023
CBC4978	212650	7048775	77.5483	-90	0	28	13	22	9	1.1	2.3	4.3	2023
CBC4979	212550	7048775	80.2296	-90	0	28	7	27	20	1.0	3.0	2.4	2023
CBC4980	212450	7048775	79.2269	-90	0	29	9	17	8	0.9	1.1	2.4	2023
CBC4981	213276.57	7048650.5	77.9976	-90	0	42	38	41	3	1.1	7.6	20.2	2023
CBC4982	213178.4	7048648.4	79.4308	-90	0	45	29	45	16	1.1	8.8	4.3	2023
CBC4983	213077.06	7048645.2	80.6356	-90	0	47	11	43	32	1.2	1.9	0.9	2023
CBC4984	212975.72	7048643.1	76.8423	-90	0	40	28	36	8	1.2	1.4	2.2	2023
CBC4985	212875.65	7048634.7	72.306	-90	0	36	20	34	14	1.3	2.2	2.4	2023
CBC4986	212775.65	7048634.7	69.0687	-90	0	39	19	27	8	1.4	3.8	1.4	2023
CBC4987	212675.65	7048634.7	67.5201	-90	0	34	11	27	16	0.9	1.5	1.3	2023
CBC4989	212475.65	7048634.7	67.6385	-90	0	31	15	24	9	0.9	1.0	1.1	2023
CBC4990	213250	7048525	90.6728	-90	0	42	24	36	12	1.2	3.1	2.2	2023
CBC4991	213200	7048525	91.3996	-90	0	39	26	39	13	1.3	3.0	2.6	2023
CBC4992	213150	7048525	92.4397	-90	0	40	28	40	12	2.0	4.8	3.6	2023
CBC4993	213100	7048525	92.7714	-90	0	40	27	39	12	2.3	3.1	1.0	2023